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WAVELET FEATURES FOR FAILURE
DETECTION AND IDENTIFICATION
IN VIBRATING SYSTEMS

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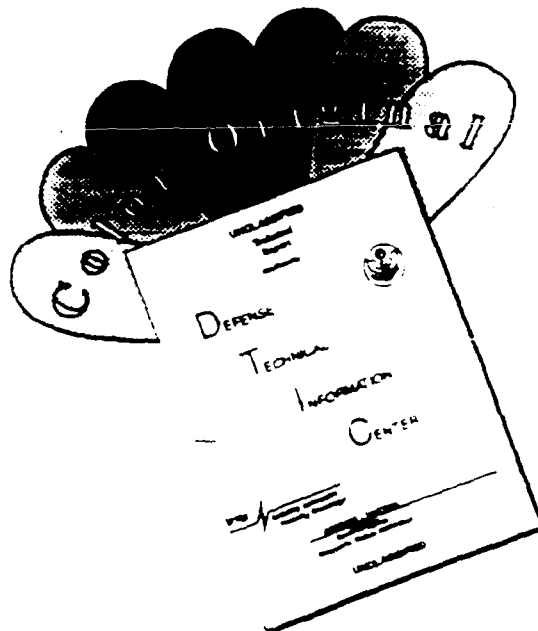
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| 13. ABSTRACT (Maximum 200 words) <p>The result of this effort is an extremely flexible and powerful methodology for failure detection and identification (FDI) in vibrating systems. The essential elements of this methodology are: 1) an off-line set of techniques to <i>identify</i> high-energy, statistically significant features in the continuous wavelet transform (CWT); 2) a CWT-based preprocessor to <i>extract</i> the most useful features from the sensor signal; and 3) simple artificial neural networks (incorporating a mechanism to defer any decision if the current feature sample is determined to be ambiguous) for the subsequent <i>classification</i> task. For the helicopter intermediate gearbox test-stand data and centrifugal and fire pump shipboard (mild operating condition) data used in this study, the algorithms designed using this method achieved <i>perfect detection performance</i> (1.000 probability of detection, and 0.000 false alarm probability), with a probability < .04 that a decision would be deferred—based on only 500 milliseconds of data from each sample case.</p> <p>While this effort shows the exceptional promise of our wavelet-based method for FDI in vibrating systems, more demanding applications, which also have other sources of high-energy vibration, raise additional technical issues that could provide the focus for a Phase II effort.</p> | | | | |
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EXECUTIVE SUMMARY

This report contains the results of a Phase I Small Business Innovative Research project funded by DARPA in Topic 92-049, Wavelets and Failure Prediction. The objectives of this project were: 1) to assess the efficacy of wavelet techniques to select features upon which simple and reliable classifiers could base decisions regarding abnormal changes in system behavior, and 2) to develop and test an algorithm for the detection of failures in vibrating systems such as gearboxes and pumps. For reliable and robust classification with low false alarm rates, the selected features must be *robust* and *maximally informative*. That is, these features must: 1) reliably persist in the presence of noise and disturbances, and also 2) provide maximally distinguishable characteristics for the detection and classification of failure modes. In this effort, we have achieved these objectives, and have also developed and tested the preliminary version of a failure detection methodology that is computationally simple, reliable, and robust.

Wavelets offer several different ways to access the structure of a signal in time and frequency. In this project, we found that the *continuous wavelet transform* (CWT) provided an ideal tool to identify significant features for fault detection in vibrating systems such as gearboxes, and to provide the basis for extracting those features. Like other image-visualization techniques such as the short-term discrete Fourier transform (DFT), the CWT converts a one-dimensional signal into a two-dimensional image. However, the CWT eliminates windowing artifacts and provides more flexibility to trade time resolution for frequency resolution. In the CWT, each line of the image corresponds to the time series response of one of the filters in a constant-Q filter bank driven by the observed sensor data. This filter bank provides complete coverage of time and frequency behavior. The resulting CWT image provides an extremely useful visualizaion of the structure of the sensor signals; by comparing images from varying conditions, one can identify a comparatively small number of features that are robust and maximally informative.

The ability to visually identify critical features during the algorithm *design* phase leads to a second, even more important consequence in the *implementation* phase: *it makes the job of the adaptive classifier far easier*. Because so much of the signal structure is obvious, and because the need for robust features leads one to focus only on high-energy areas of the CWT images, the number of features needed for classification can be astonishingly small. In comparison to feature sets based on the Discrete Fourier Transform, which may have from 256 to 16384 elements in a feature vector for the faulty systems examined here, we found that less than 20 features sufficed to obtain reliable separation among classes for the gearbox and pump data available to this effort. Small feature sets lead to extremely simple three-layer artificial neural network (ANN) classifiers—in the order of 50 processing elements—which could then be designed with noteworthy ease and without the need for exotic training algorithms. Also, the amount of data needed to train such simple nets is quite small—we were able to train classifiers using only 500 milliseconds of data from each sample case.

The result of this effort is an extremely flexible and powerful methodology to exploit the power of wavelet techniques to detect failures in vibrating systems. The essential elements of this methodology are: 1) an off-line set of techniques to identify high energy, statistically significant features in the CWT; 2) a wavelet-based preprocessor to extract the most useful features from the sensor signal, and 3) simple ANNs (incorporating a decision-deferral mechanism to defer any decision if the current feature sample is determined to be ambiguous) for the subsequent classification task. In the gearbox and pump data sets used in this study, the algorithms designed using this method achieved *perfect detection performance* (1.000 probability of detection, and 0.000 false alarm probability), with a probability $< .04$ that a decision would be deferred for a few milliseconds—again based on only 500 milliseconds of data from each sample case.

While the full CWT may represent a significant computational requirement, it is only used in the off-line *design phase* to identify critical features. The final implementation of a fault detection system consists of a comparatively simple wavelet-based preprocessor (probably implementable as a single-chip custom integrated circuit, at least for audio frequency processing),

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followed by a very simple ANN—a configuration ideally suited to real-time implementation using either digital *or* analog hardware.

This effort shows the exceptional promise of our wavelet-based method for failure detection in vibrating systems. There is no known impediment to fielding this technology within an additional 24 months for simple systems such as terrestrial pumps, electrical machinery, or engines. However, more demanding applications, such as machinery (gearboxes) mounted on moving platforms (helicopters) that have other sources of high-energy vibration (engines), raise some additional technical issues that could provide the focus for a Phase II effort.

In particular, the data used in Phase I was taken from a test stand or under mild operating conditions, and thus does not display the full array of *environmental disturbances and exogenous sources of vibration* that will make applications to helicopter gearboxes more difficult—the fault detector must be able to separate unexpected variations in environmental vibrations from unexpected changes in the gearbox which may indicate a developing failure. Thus one must expand substantially the set of conditions under which data has been collected to include the full ranging of operating conditions.

To counter the additional complexity offered by uncontrolled environmental vibrations, there are two critical ways in which performance of our methods can be significantly enhanced. (While such enhancements were completely unnecessary for the data sets used in Phase I, we fully expect that they would be needed in an operational helicopter environment.) Specifically, throughout the Phase I effort only *a single channel of sensor data* was used in any of the algorithm designs and tests. However, typically there will be several sensor sets available for processing (e.g. for the data used in Phase I there were two accelerometer channels). In the comparatively benign environment of test stand data, one channel proved sufficient for robust and reliable detection performance, but in an operational environment, one would expect that achieving such reliable performance would require the combined use of all sensor channels in an integrated system in which wavelet-based features are extracted jointly from the full set of channels. Intuitively, some sensors may provide information on background vibrations that may mask or interfere with

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the features crucial to fault detection, and this background must be taken into account during on-line feature extraction. In particular, phase differences between the CWTs of case- and support-mounted sensors may provide significant information concerning the physical origin of the vibrations at each frequency of interest.

In addition, one would also expect that other helicopter system sensors might be of considerable use in providing *situational data*, i.e., to identify environmental conditions and other vibrational sources influencing the gearbox sensors, thus providing useful inputs to the failure detection algorithm. For example, one could adapt the classification thresholds and parameters to the amount of torque applied by the engines to the drive shafts (which affects both the intensity and harmonic structure of a gearbox signal), or to gross flight conditions (e.g., grounded, vertical ascent, hovering, cruise, etc.)

In addition to these enhancements, there are also several other issues of some importance to an operational design. One such issue is the context in which the fault detection system is to operate. For example, is the goal simply to *detect* failure, or is detailed *failure diagnosis* desired in order to guide maintenance activities? What response time is needed for the detection system in order to avoid catastrophic failure? Requirements for system-level objectives such as these will obviously be needed in setting algorithm parameters and for assessing overall performance against these objectives.

Just as obviously, the practical implementation of the algorithm must be considered. Indeed, as we have indicated, our algorithms appear to be suited to either digital or analog implementation, and the issues of sizing, computational speed requirements, etc., would need to be considered.

Thus there is much to do in order to turn these results into a final product suitable for flight testing on operational helicopters. However, the exceptional performance achieved in Phase I clearly indicates that the potential of our wavelet-based failure detection method merits the additional effort required to realize it.

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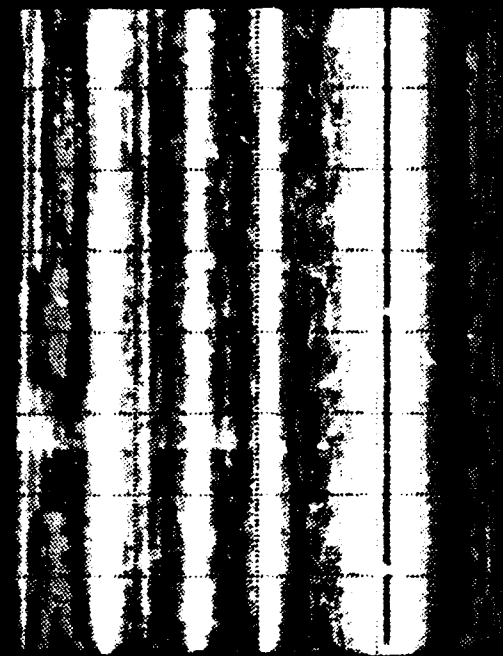
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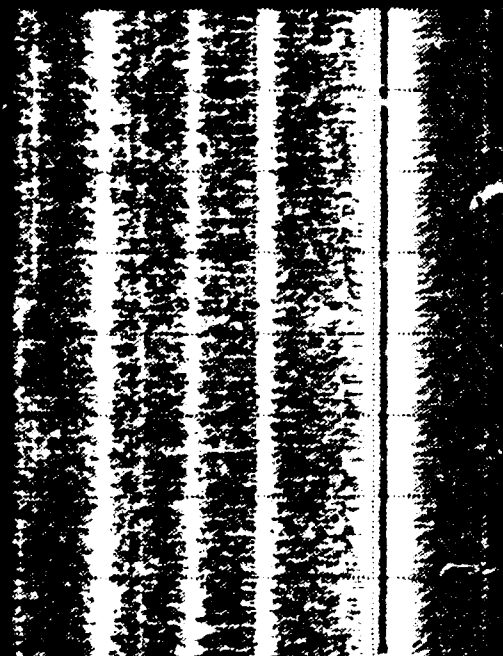
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16 kHz

4 kHz

1 kHz



256 Hz

64 Hz

125 msec 250 msec 375 msec 125 msec 250 msec 375 msec

Plate A Effect of Smoothing the Continuous Wavelet Transform

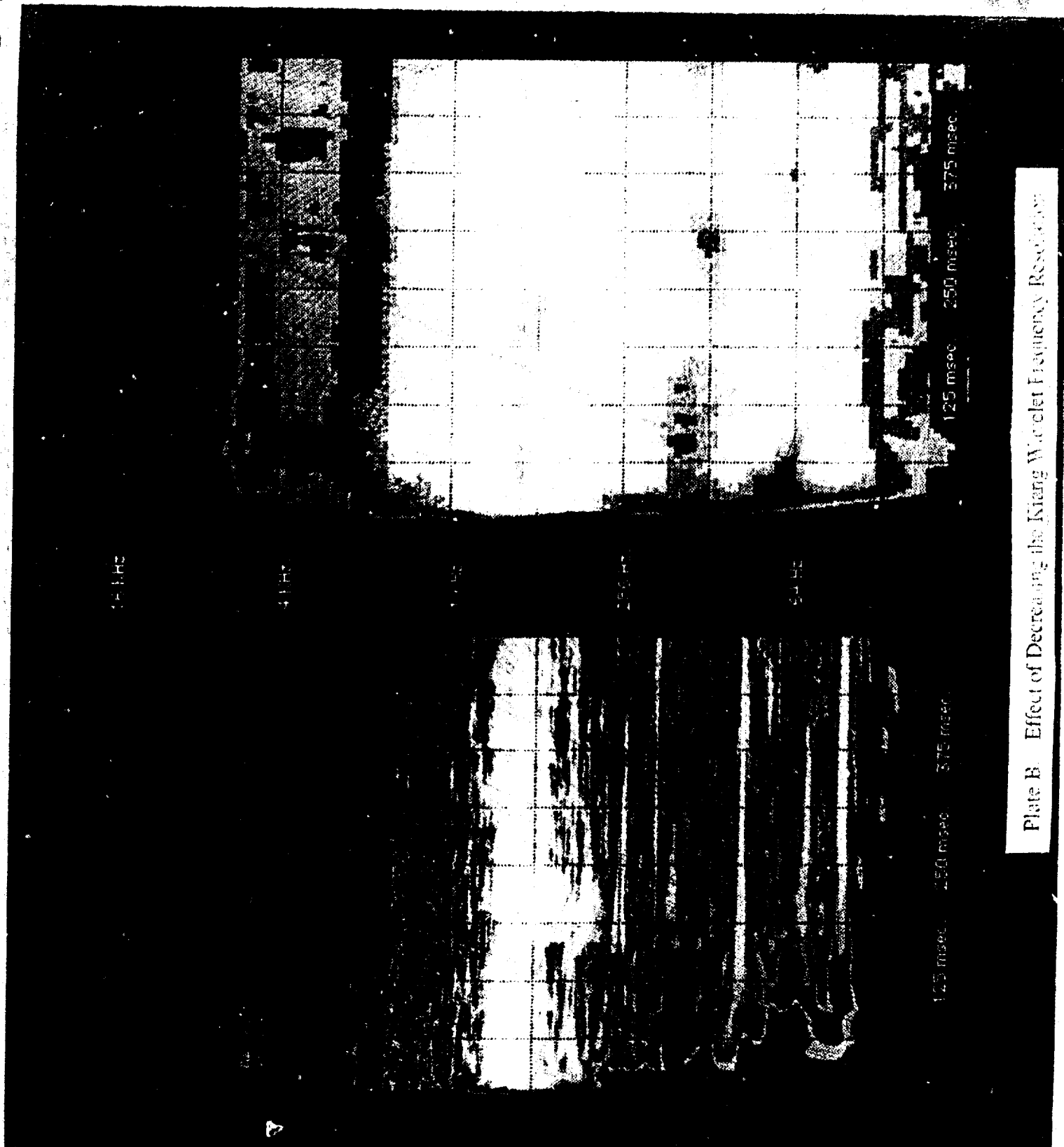


Plate B Effect of Decreasing the Kiang Woodlet Frequency Resolution

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16 kHz

4 kHz

1 kHz

256 Hz

64 Hz

125 msec 250 msec 375 msec

125 msec 250 msec 375 msec

Plate C. Condensate Pump Axial and Radial Data Channels in the CWT Domain

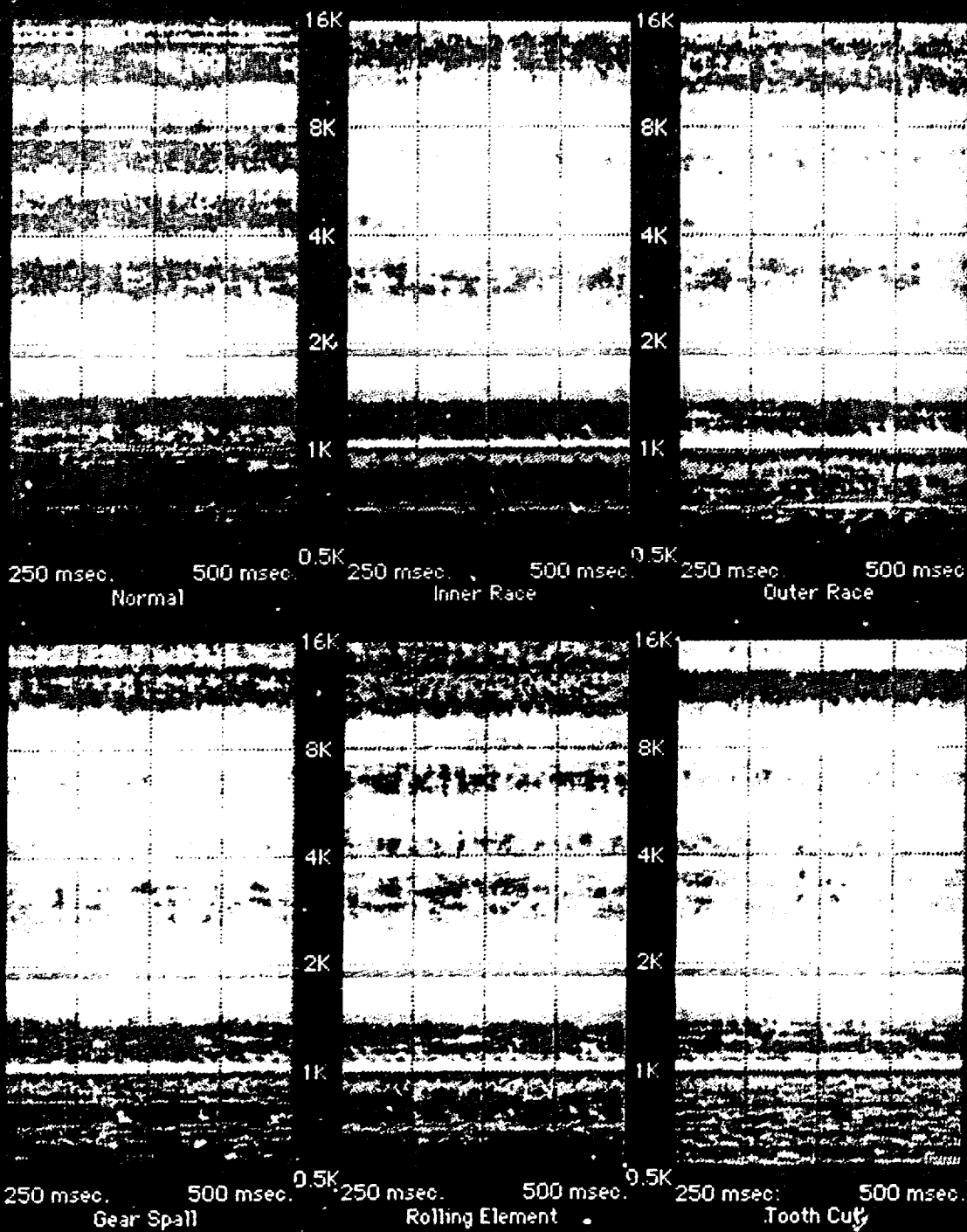


Plate D Channel 5 Helicopter Gearbox Fault Condition Signatures in the C-A-T Domain

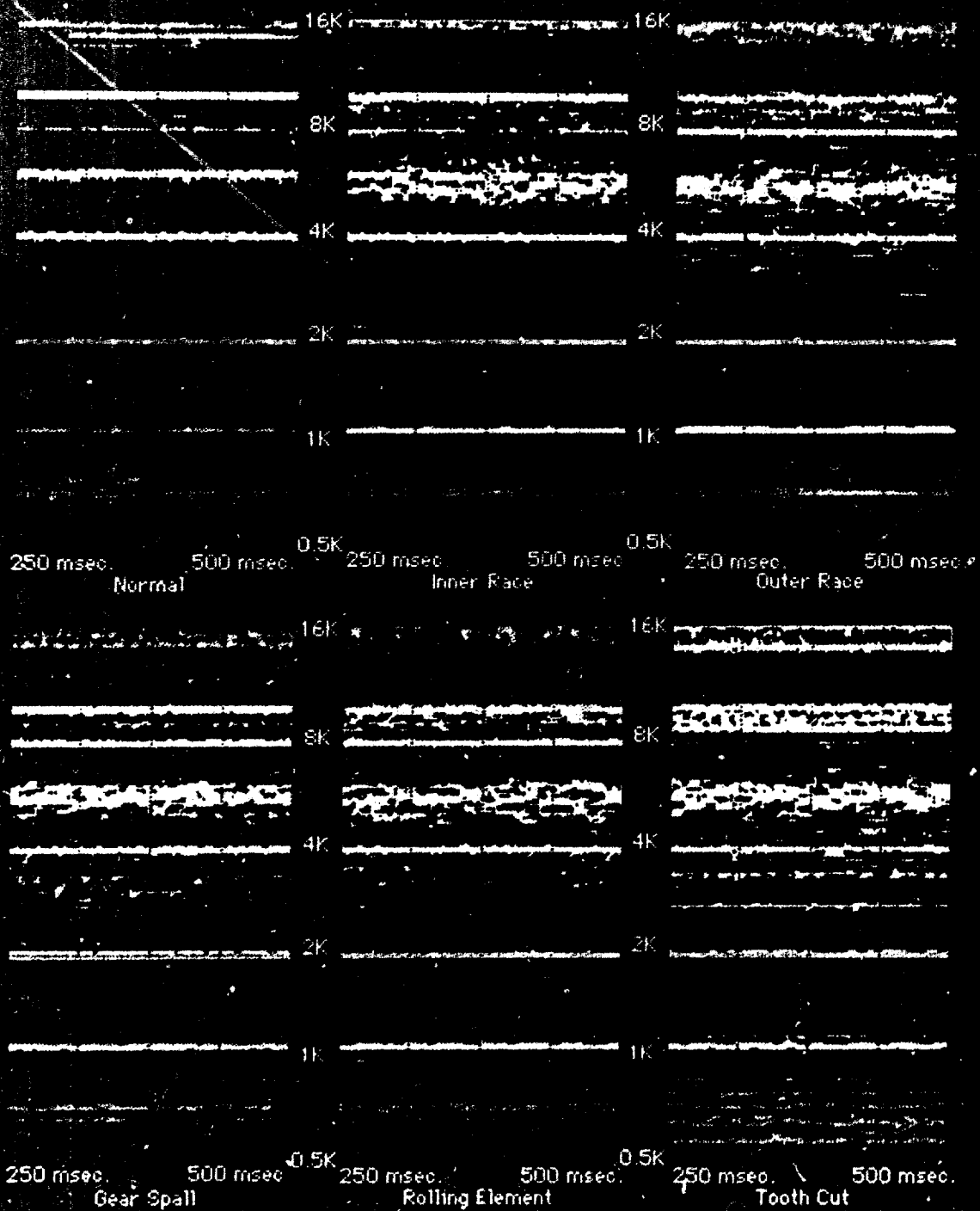


Plate F. Channel 5 Helicopter Gearbox Signatures After Making Low Level Flight

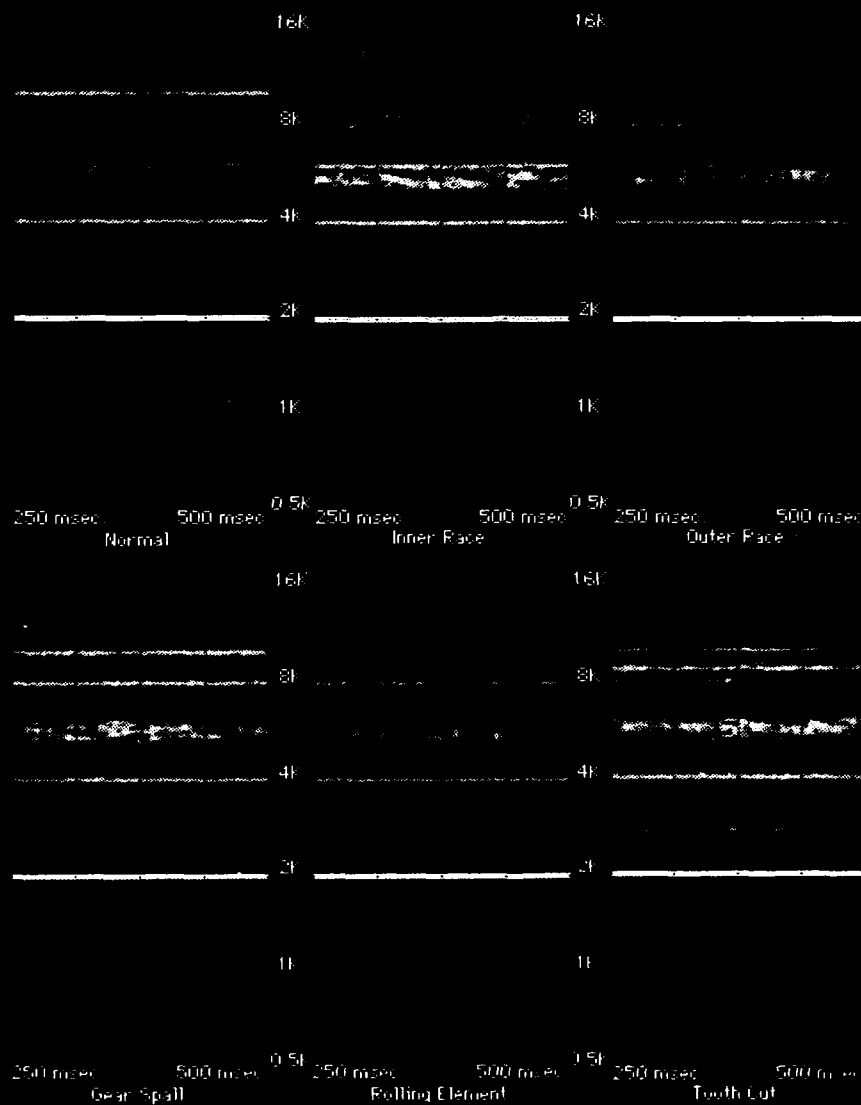
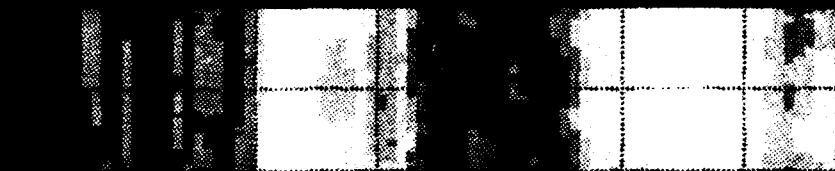


Plate G. Channel 6 Helicopter Gearbox Signatures After Masking Out Low-Level Energy

Condensate Pumps



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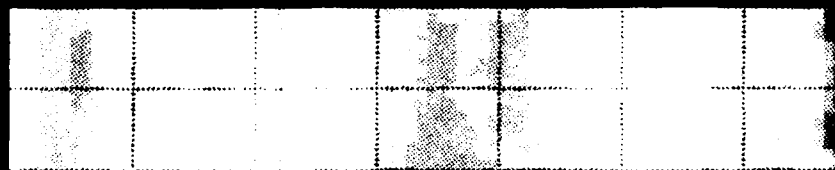
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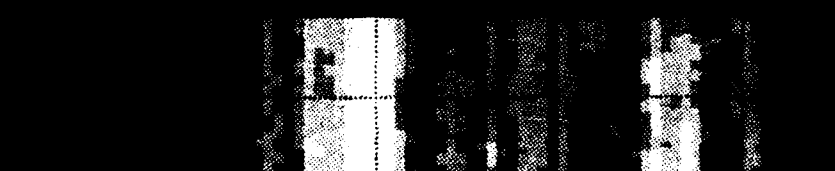
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16 Hz

64 Hz

256 Hz

1 kHz

4 kHz

16 kHz

Plate H. Condensate Pump Signatures in the CWT Domain

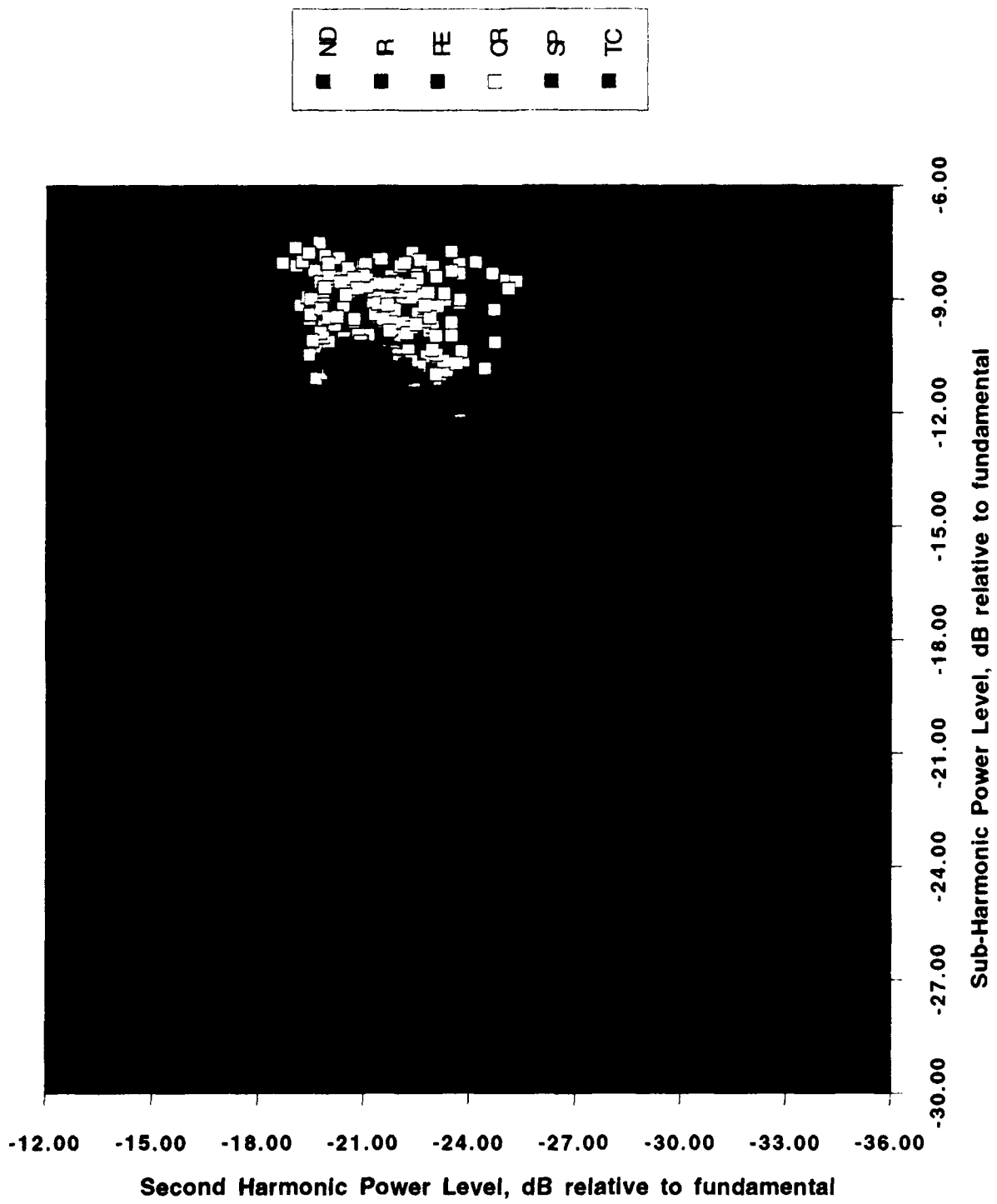


Plate I. Helicopter Gearbox Feature Cluster Separation

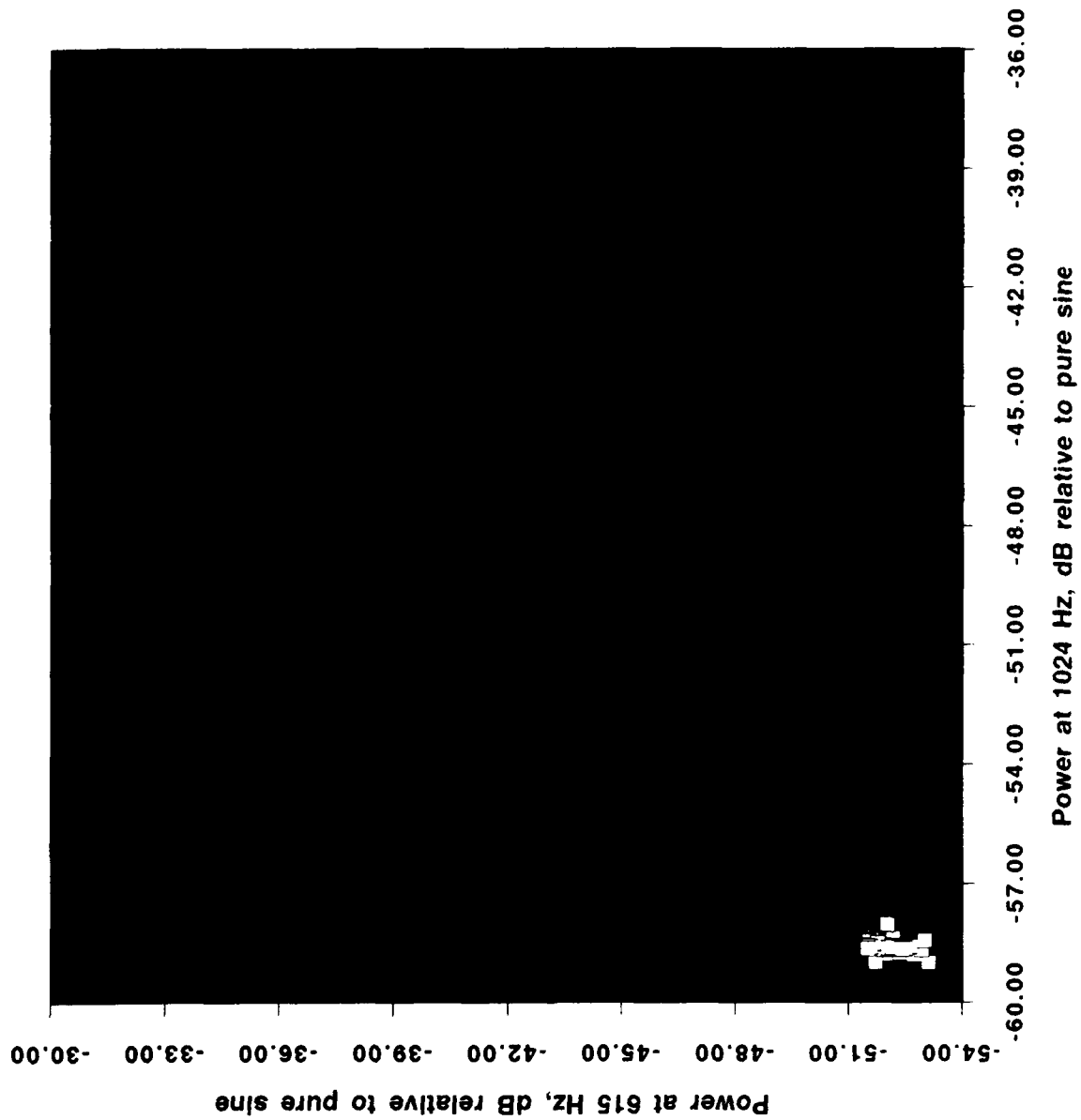


Plate J. Condensate Pump Feature Cluster Separation

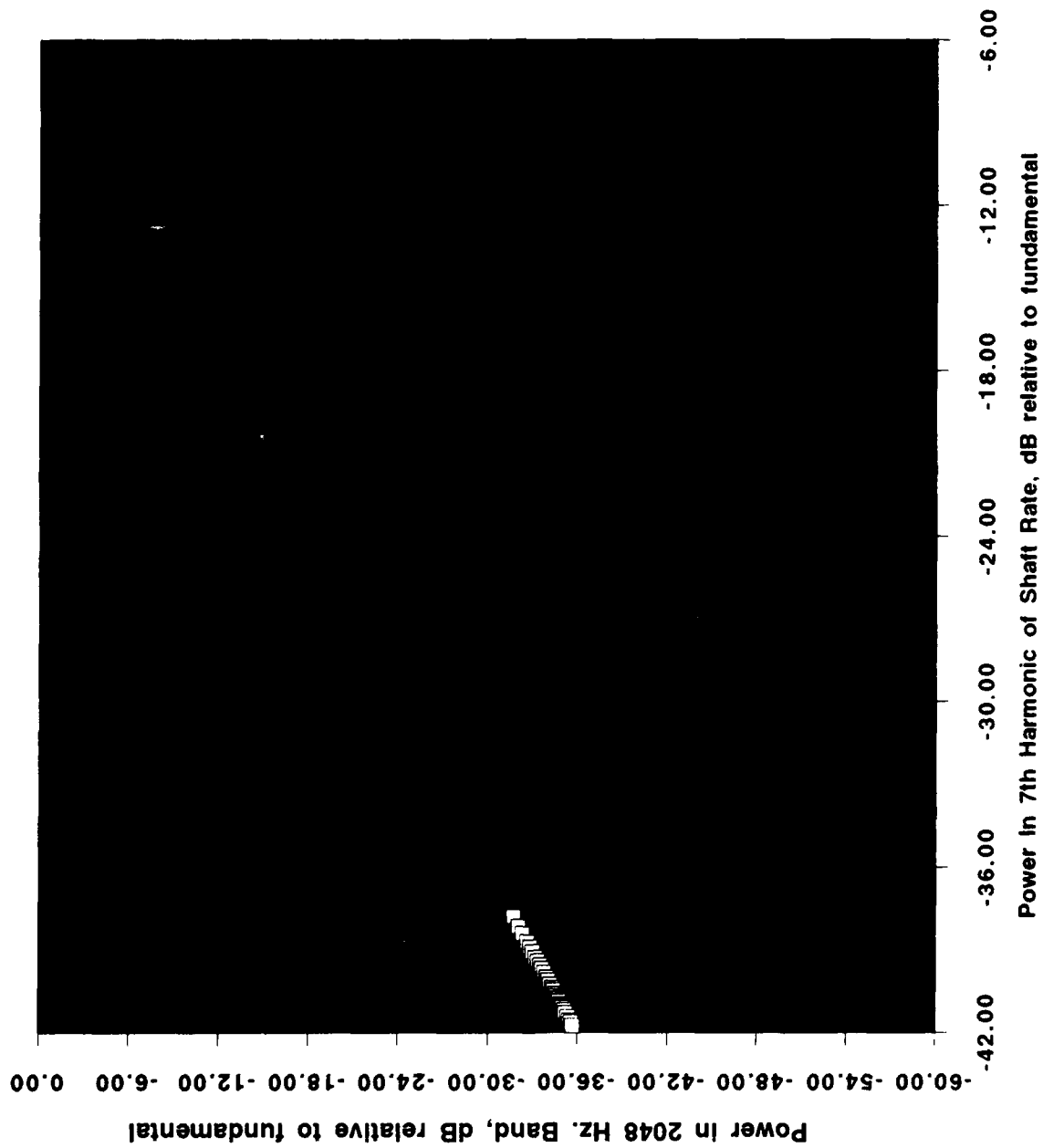


Plate K. Fire Pump Feature Cluster Separation

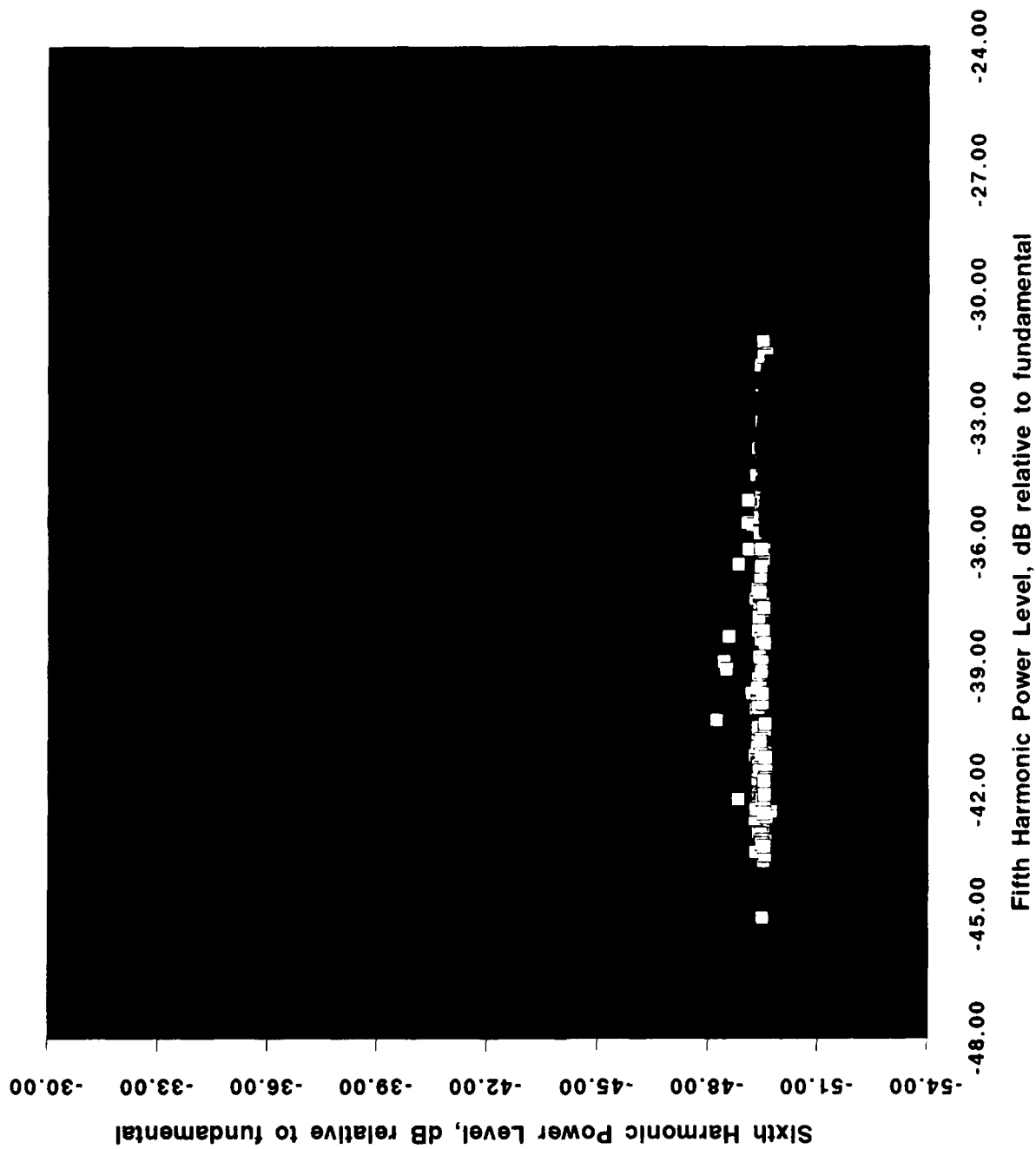


Plate L. Artifacts in Training Data—Helicopter Gearbox



Plate M. Cornelian Window blind, and a fold, and a view.

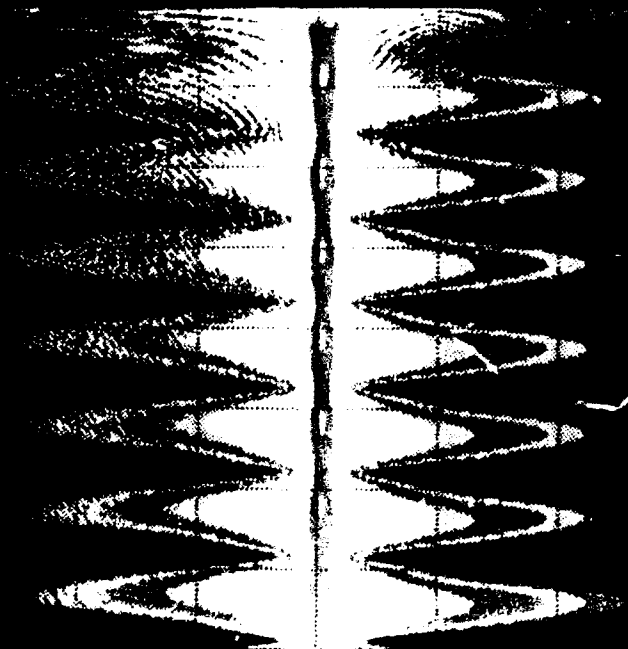
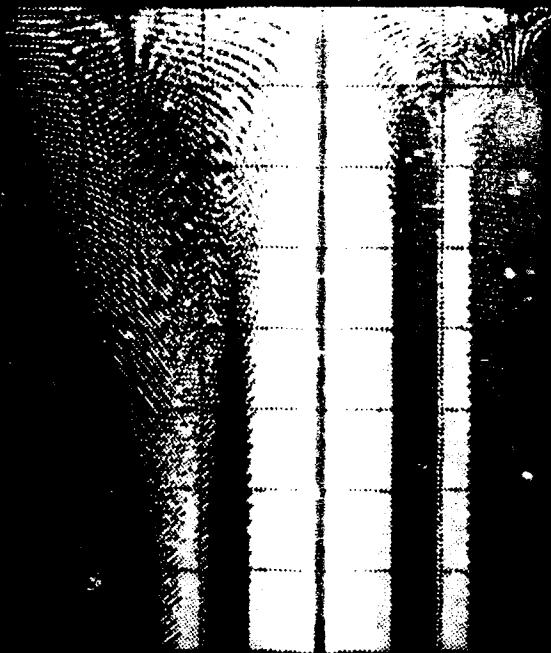
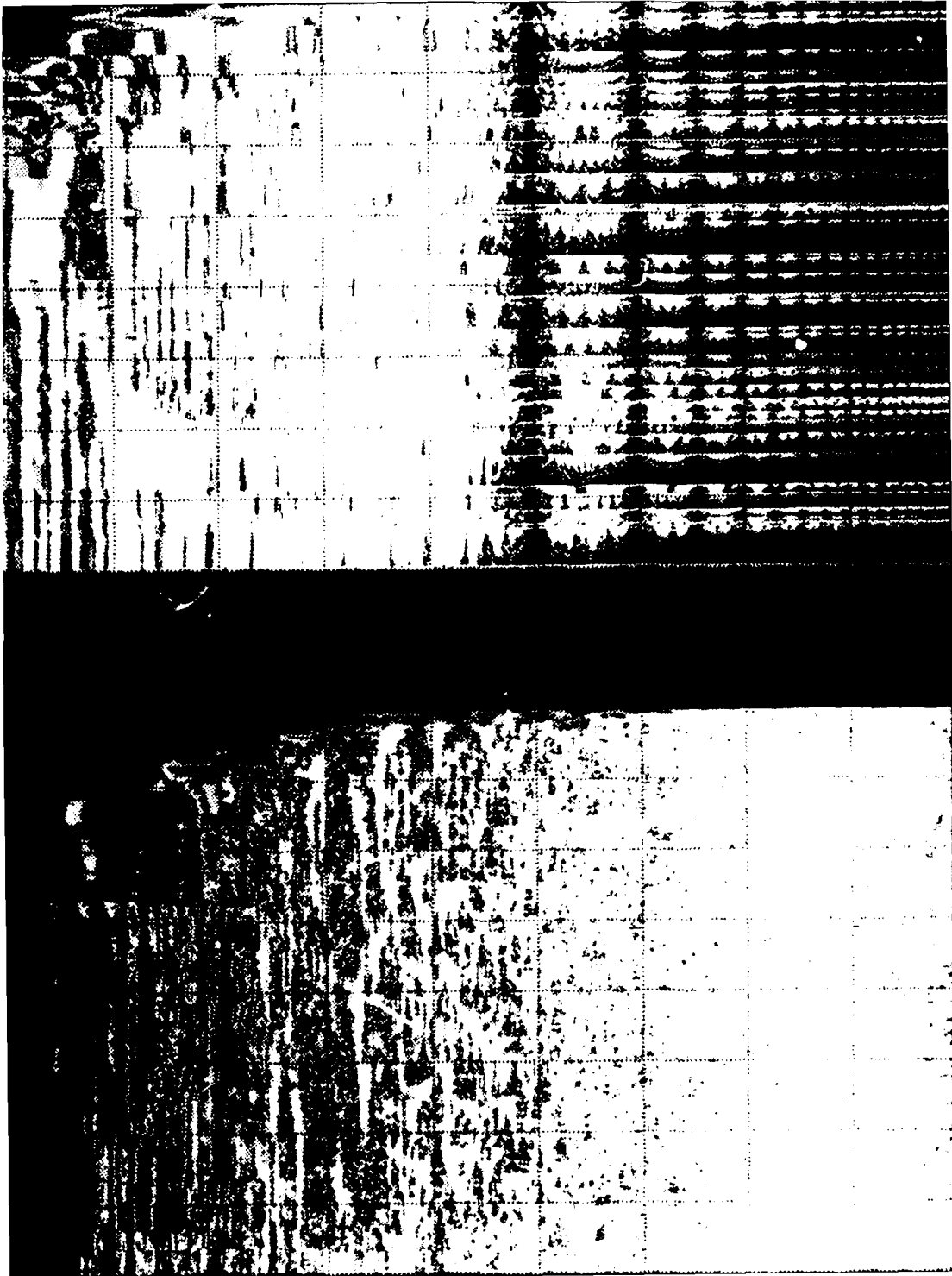


Plate N. Continue. Western Ironstone, at F. de la Plata, Sonora, Mexico.



SECTION 1

INTRODUCTION

This report presents the results of a Phase I Small Business Innovation Research project funded by DARPA in Topic 92-049, Wavelets and Failure Prediction. Recommendations for a Phase II follow-on are also included.

1.1 IDENTIFICATION AND SIGNIFICANCE OF THE PROBLEM

The timely and reliable detection of changes in the dynamic behavior of complex systems and signals is a problem of considerable importance in a vast array of military and civilian applications. As we continue to place increasingly demanding objectives on system performance, cost, and reliability, the needs for and requirements on such detection methods grow commensurately. For example, the increasing role of and reliance on computer control—for the fly-by-wire control of advanced high-performance aircraft and helicopters, the navigation of autonomous vehicles, etc.—makes the detection of system anomalies essential, since by their very nature such automatic systems simply do not have the luxury of relying on the extraordinary but workload-limited detection capabilities of their human pilots. Also, the cost of modern-day military systems are such that there are tremendous payoffs to be gained if the availability of a weapons system is improved, or its life cycle cost reduced.

These objectives provided much of the motivation for the development of self-repairing flight control system concepts (Weiss and Hsu, 1987) for the in-flight detection of battle damage and sensor and actuator failures in advanced aircraft in order: 1) to facilitate control system reconfiguration to allow mission completion (or at least the safe return of the vehicle), and 2) to provide early diagnosis of problems that could then speed up the maintenance process and reduce turn-around time.

Furthermore, the reliable detection of component damage or failure can have a dramatic effect on the cost of maintaining and/or replacing an advanced military vehicle such as a helicopter, ship, fighter, or even unmanned vehicles. Specifically, the total cost of such a system is so high that the objective of avoiding system loss due to an undetected failure in some component places severe demands on the overall reliability of components and their monitoring systems.

Moreover, this need for reliability has typically led to extremely conservative maintenance and replacement procedures: components are automatically replaced after time in service reaches a prescribed limit, usually taken to be significantly less than their expected failure times. Thus the availability of advanced and reliable fault detection systems offers the promise not only of improved system reliability but also the possibility of increasing component time in service by detecting the onset of problems and thus allowing "retirement for cause" rather than the more expensive present practice of replacing components whether they need it or not.

These and a variety of other factors and applications have led to considerable research and development activity over the past 20 years resulting in an array of detection and diagnosis methods (see, for example, the widely referenced surveys Willsky (1976) and Basseville (1987)) providing us with an analytically sound, proven-in-practice foundation from which to pursue the new challenges arising as we push harder on the envelope of performance, reliability, and cost. Moreover, in the past few years significant new methods of signal analysis and pattern recognition (in particular, wavelet transforms and artificial neural networks) have been developed offering the promise of adding significantly to the arsenal of detection methods and to the range of applications that can be dealt with successfully.

1.2 OBJECTIVES OF PHASE I

The objective of the Phase I effort was to assess the efficacy of wavelet techniques for selecting *features* upon which an adaptive classifier could base its decisions regarding abnormal changes in system behavior. For reliable, robust classification with low false alarm rates, these features must be:

- *high energy* in at least one case (normal or failed) in order to persist reliably even in the presence of environmental noises or transient disturbances; and
- *statistically significant* in separating two or more cases from one another in order to contribute meaningful information to the pattern classifier.

Our objective was not to develop new classification techniques, but rather to modify off-the-shelf artificial neural network (ANN) (Lau and Widrow, 1990a, 1990b) technology as needed to integrate it with a front-end feature extractor based on wavelet techniques.

Wavelets offer many different ways to access the structure of a signal in time/scale space. The *continuous wavelet transform* (CWT) (Ruskai, Beylkin, et al., 1992; Daubechies, 1990; Mallat, 1989a, 1989b; Meyer, 1988) converts a time signal into an image, from which features can be extracted using image processing techniques. The *wavelet packet transform* (WPT) (Coifman and Wickerhauser, 1992; Coifman et al., 1990) derives coefficients of wavelet basis functions that characterize time/scale energy distribution in a much more flexible manner than *discrete Fourier transforms* (DFTs) permit. Variations on the WPT permit the selection of subsets of an overcomplete set of basis functions to find the most significant elements of a signal. More recent extensions to wavelet techniques, presented under the general classification of multiscale signal processing, create even more options for feature characterization. Our initial goal was to select several alternatives, and to compare their performance and computational requirements in the context of whatever data were available. As the effort progressed, we focussed our attention on CWTs and WPTs.

Because the dominant challenge in failure detection problems is to identify a concise yet distinctive set of features on which the detection/classification process can be made to depend, our emphasis in Phase I was on the back-end of the feature-selection process, i.e., we initially assumed that the full set of wavelet transform coefficients was already available, and then determined *which subset was most critical* to good performance of an ANN classifier. Helicopter gearbox and shipboard pump accelerometer data, supplied by the Navy, were passed through a CWT and WPT preprocessors, and then used to train ANN classifiers. Statistics on false alarm

rates, miss detections, and misclassification errors were used to quantify the performance of the proposed methodology.

1.3 OVERVIEW OF PHASE I RESULTS

Phase I of this effort clearly demonstrated the feasibility of incipient fault detection for vibrating systems not only for bench test conditions (helicopter gearbox) but also for mild operating conditions (condensate and fire pumps). Remarkable Phase I results were obtained by using a balanced combination of CWTs and ANNs. We used the CWT to select features for an ANN classifier. The wavelet transform provided enough visibility into fault signals to allow us to reduce the size of the feature set to 10-15 features. We used a low-dimensional, conventional ANN classifier (Widrow et al., 1988) with rejection of ambiguous classifications. We achieved 0.000 probability of false alarm, 0.000 probability of missed detection, and < 0.04 probability of deferral (to a subsequent feature vector) for all three data sets provided by the Navy. The major product of our Phase I work is a single methodology to identify robust features that lead to these performance levels.

1.4 REPORT ORGANIZATION

Section 2 describes the major components of the technical approach and the main results of this Phase I effort. Section 3 presents the main conclusions and recommendations for future effort. Appendix A contains an overview of the CWT and presents some examples to give the reader insight into the time-frequency information provided by the CWT based on the Kiang wavelet used in this work. Appendix B provides some mathematical background on the CWT.

SECTION 2

PHASE I TECHNICAL EFFORT

This section describes the data used, the major components of the technical approach, and the main results obtained for the three types of vibrating systems considered in this work. The most important steps of the technical approach are illustrated with selected examples based on the available data sets and using the color plates located just before the body of this report.

2.1 DATA USED IN PHASE I

For this research the Naval Command, Control, and Ocean Surveillance Center (NCCOSC) supplied data for three vibrating systems: helicopter gearbox, condensate pumps, and fire pumps. These data are from accelerometers that measure vibrations at one or more places on the case of the vibrating mechanism.

The gearbox data (from a relatively simple TH-1L helicopter intermediate 42-degree gearbox, illustrated in Fig. 2-1) consisted of vibration readings (sampled at 48 kHz) from two accelerometers (channels 5 and 6, oriented with and orthogonal to the bearing load zones, respectively) mounted on the gearbox output end for six separate fault conditions: no defect (ND), bearing inner race fault (IR), bearing rolling element fault (RE), bearing outer race fault (OR), gear spall fault (SP), and gear 1/2 tooth cut fault (TC). This is a subset of the "Hollins data base," developed by Mark Hollins of the Naval Air Test Center (NATC). The pump data consisted of vibration readings (sampled at 50 kHz) from two triaxial accelerometers (axial, radial, tangential channels were available) mounted on the motor and pump ends of the assembly, one triad on each end. The condensate pump data consisted of eight data segments that included two fault types and four unfailed units. The fire pump data consisted of 16 data segments that included four fault types and eleven unfailed units. Unlike the helicopter data, which are bench test data with seeded faults, the pump data were obtained from shipboard pumps operating under relatively mild conditions.

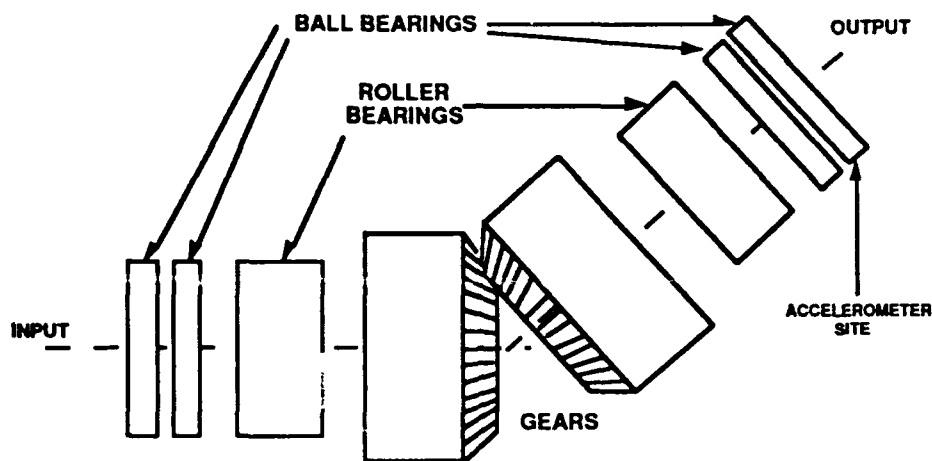


Figure 2-1. Illustration of Intermediate Gearbox

Tables 2-1 and 2-2 present the information available on the condensate and fire pump data, respectively. In both cases, fault code 0 is used to label good pumps (normal cases). Also, fire pump fault codes 3B and 4A denote the same fault type on different pumps.

TABLE 2-1. CONDENSATE PUMP INFORMATION

| Segment Number | Pump ID | Fault Code | RPM |
|----------------|---------|------------|-----|
| 1 | CP-1A | 1 | 900 |
| 2 | CP-1B | 0 | 900 |
| 3 | CP-4A | 2 | 885 |
| 4 | CP-4B | 0 | 885 |
| 5 | CP-2A | 0 | 890 |
| 6 | CP-2B | 0 | 890 |
| 7 | CP-3A | 0 | 892 |
| 8 | CP-3B | 2 | 892 |

TABLE 2-2. FIRE PUMP INFORMATION

| Segment Number | Pump ID | Fault Code | RPM |
|----------------|---------|------------|------|
| 1 | FP-9 | 3A | 3576 |
| 2 | FP-3 | 0 | 3585 |
| 3 | FP-2 | 0 | 3585 |
| 4 | FP-1 | 0 | 3585 |
| 5 | FP-4 | 0 | 3575 |
| 6 | FP-5 | 0 | 3580 |

| | | | |
|----|--------|----|------|
| 7 | FP-6 | 0 | 3580 |
| 8 | FP-5A | 0 | 3585 |
| 9 | FP-6A | 4 | 3580 |
| 10 | FP-13A | 0 | 3590 |
| 11 | FP-12 | 5 | 3585 |
| 12 | FP-13 | 3B | 3580 |
| 13 | FP-14 | 6 | 3570 |
| 14 | FP-17 | 0 | 3585 |
| 15 | FP-16 | 0 | 3585 |
| 16 | FP-15 | 0 | 3588 |

For our test systems we used only one channel, from one sensor—we deferred fusion of results from multichannel data to Phase II. For the gearbox system, only channel 5 was used for all conditions. For both pump systems, only the axial component of the pump-end accelerometer triad was used. In a sense, we deliberately made the Phase I problem harder by ignoring some sources of information in order to demonstrate the power of wavelet techniques, or lack thereof, on a fault detection/classification problem more difficult than one would expect to encounter in the field under more severe conditions.

2.2 SYSTEM STRUCTURE

We adopted the conventional architecture of an adaptive classifier (Fig. 2-2): a real-time preprocessor to focus the information about the state of a system into a low-dimensional feature vector, followed by an adaptive pattern analyzer to map feature vectors into detections and classifications. Our work emphasized the development of the preprocessor, using the insight offered by recent advances in the mathematics of wavelets.

Our Phase I proposal indicated that our approach of choice was to use the WPT (Coifman and Wickerhauser, 1992; Coifman, Meyer, et al.; 1990) to identify locations in time/scale space indicative of faults. This approach met with less than expected success. With hindsight, coupled with analysis of considerable performance data generated during the project, we believe that the WPT is most appropriate for problems where classification depends on the timing and internal

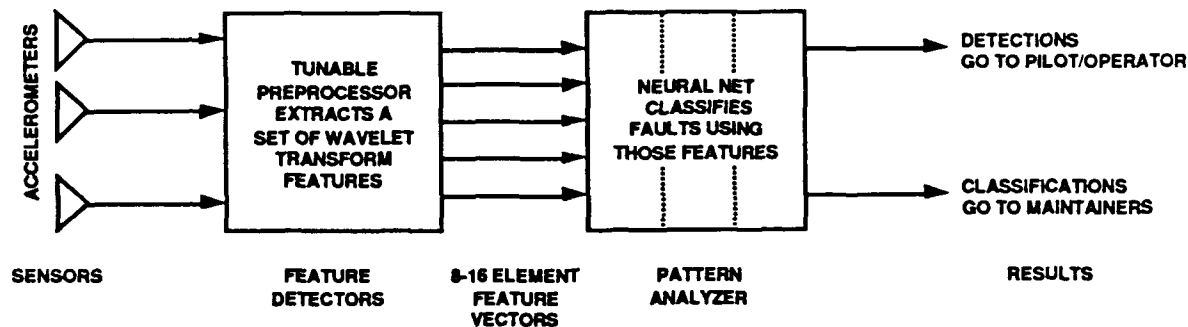


Figure 2-2. Incipient Fault Detection and Classification System Structure

structure of *transient* events, such as classifying biological sounds in the sea. They offer considerably less advantage in fault analysis of vibrating systems, where the signatures are of relatively long duration and statistically quite stationary. However, we reserve interest in the WPT for detecting incipient faults in systems that emit transient signals as part of their normal operation (e.g., heavy duty mechanical or electrical switching systems).

As an alternative, we turned to the CWT. Like other image-visualization techniques such as the Discrete Fourier Transform (DFT), the CWT converts a one-dimensional signal into a two-dimensional image, using substantial computational resources. Sub-bands of the CWT can be evaluated quite efficiently in a preprocessor, however. Therefore, we use the full-blown CWT during the *design process* to identify a few bands that differentiate among cases, and only implement actual feature detectors for those specific bands—to *focus the information available in a signal into a small set of features*. This allows us to find very small feature vectors (of the order of 10 – 20 elements) that nonetheless yield outstanding detection and classification performance. A brief explanation of the CWT and examples of the CWTs of elementary signals are presented in Appendix A.

For the pattern analyzer, we used conventional three-level, feedforward ANNs. As will be seen, we succeeded in finding feature sets that are nearly convex and linearly separable, so we did not need complex network topologies or exotic training algorithms. (In fact, we were able to set the number of elements in the hidden layer equal to the number of output elements).

To improve performance we suppressed classification results entirely if the maximum output value was less than some multiple of the next larger output value, *deferring* the classification to the next available feature vector. We could trade deferral rate for false alarm/missed detection performance by changing this multiple. A multiple of 2.0 was adequate to eliminate all false alarms and missed detections, and kept the deferral rate below 4%.

The Phase I feature-selection process used a number of tools to develop feature sets. KHOROS signal processing routines (KHOROS Group, 1992), on a SUN computer, supported editing and preliminary analysis of raw data files. A custom Macintosh Pascal package computed the CWT, and another one extracted the selected feature vectors from the raw data. Excel, a commercial package from Microsoft, supported the statistical cluster analysis. Macintosh NeuralWorks, a commercial package from NeuralWare, was used to carry out the ANN training and testing. MATLAB, a commercial package from The Math Works, Inc., was used to compute performance metrics.

2.3 WAVELET-BASED TUNABLE PREPROCESSOR

Figure 2-3 presents the wavelet-based tunable feature extractor developed in this Phase I effort. The CWT is computed using the Kiang wavelet¹, which allows one to select appropriate frequency and time resolutions to extract from the CWT the features of interest. To eliminate clutter and "spectral speckle" from the CWT, we smooth and decimate the CWT before extracting the features of interest. These bands are then parameterized to achieve better feature separability. Because of the properties of this wavelet-based feature extractor, it is not necessary to compute the entire CWT to extract a few features; only the frequency bands associated with the features of interest need to be computed. This leads to a significant reduction of computational effort if the number of selected features is relatively small (say, 10 to 20). (Note that while this preprocessor is currently implemented in software, it is a good candidate for hardware implementation—on a

¹ Named after Nelson Kiang of MIT, who derived tuning curves for auditory nerve neurons in the middle 1960's. For this project, we selected a mother wavelet whose Fourier transform closely matches these tuning curves.

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Macintosh Quadra 900 computer, with no optimization, it runs about 100 times slower than real time.)

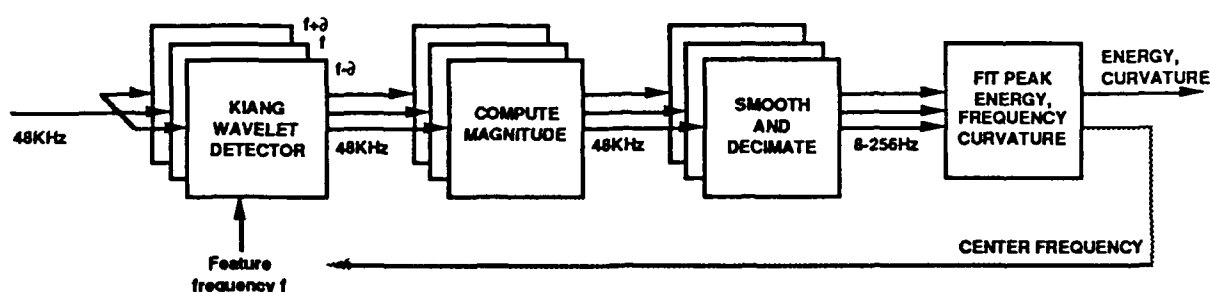


Figure 2-3. Tunable Feature Extractor

As our emphasis in Phase I was on the selection of a concise, focused feature set, we employed the visibility into time/scale space offered by the CWT. Our objective was to focus all of the potentially available time/frequency information into a small feature space, since a small, separable feature set reduces the complexity required of a classifier, and hence the risk of slow or non-convergence.

Another advantage of the CWT is its ability to isolate robust high-energy features that can be readily detected and can be suppressed only with a great deal of external energy. Our approach to feature selection was explicitly to ignore regions of time/scale space with consistently low energy, on the grounds that whatever classification might be possible using such features would not be robust to disturbances. (However, we did include one low-energy band specifically as a *disturbance detector*, where classifications would be suppressed whenever substantial energy appeared in this band.) We knew that bench test or mild-operation data is invariably cleaner than field data (it may not represent a complete range of normal operations or disturbances, and may contain artifacts not present in real data) and therefore we sought features that would serve as well in noisy environments as they do on these data sets. *Thus we are prepared to handle much more challenging data, since we address robustness at the very beginning of the feature-selection process.*

2.3.1 The Continuous Wavelet Transform

The CWT appears as an image. It is qualitatively similar to other imaging representations of a signal, such as sonograms, lofargrams, or waterfall displays. The biggest distinction is that one raster line appears in the image *for every sample in the signal*—there is no windowing of the data, and hence no artifacts in the image due to windowing. Minor distinctions include the fact that the scale axis is logarithmic, since wavelet theory involves continuous scaling of a single basis function. If one thinks of the discrete Fourier transform as the output of a bank of constant-bandwidth filters, then one can think of the CWT as the output of a bank of constant-Q (ratio of bandwidth to center frequency) filters. (The WPT, on the other hand, is like a variable-bandwidth, variable-Q filter bank (Vetterli and Herley, 1990).)

Visual analysis of the CWT reveals areas of interest in vibrational data. The raw CWT magnitudes include high-frequency artifacts that can be removed by smoothing over time. The helicopter data segments show high-energy, narrowband features overlaid by short disturbances resulting from the periodic clash of gear teeth and (in failed cases) the impact of bearings on defects in the bearing tracks. The pump data segments show lower-energy, broadband features overlaid by aperiodic impulsive disturbances, presumably representing flow noise and exogenous disturbances. In all cases, features appear to be stable over significant periods of time.

The CWTs presented in the color plates referenced in the sequel (and located just before the body of this document) illustrate these general observations. These CWTs use the Kiang wavelet (fine frequency, coarse time resolution). Hue encodes the log magnitude of the CWT (blue = low, red = high). Phase information is ignored. Time divisions are 62.5 msec wide. The frequency scale is logarithmic, and frequency divisions correspond to octaves.

2.3.2 Smoothing the CWT

The two images in Plate A are from the first 500 msec of channel 5 of the normal helicopter gearbox data (sampled at 48 kHz). The left image is the CWT sampled every 2 msec—the full CWT for this data segment would be 24,000 pixels high. The bright red line just below 2,048 Hz is the gear mesh fundamental. Harmonics of this fundamental appear at higher frequencies (finer

scales), although there appears to be little energy in the fourth, sixth, and seventh harmonics under normal conditions (possibly due to a zero in the transfer function between the gear assembly and the sensor site, at least in the range of the sixth and seventh harmonic). The data appears to be high-pass filtered with a cut-off frequency around 1 kHz, although some frequency lines are visible below this point.

Because faults in vibrating systems impact a sensor on every cycle of the mechanism, we seek features that persist over relatively long periods of time (many cycles). While the texture of the raw CWT between harmonic lines is interesting, it would be imprudent to attempt to classify faults based on the structure of this texture. Thus for this data set, and for all other CWT images we constructed, the image was smoothed in the time dimension to suppress high-frequency textures, and enhance the stationary elements of the signal. The right image in Plate A shows the results of this smoothing. Among other things, the smoothing enhances the appearance of a secondary line just above the mesh fundamental. Also, some 5 Hz modulation on the fifth harmonic becomes more apparent.

Note that we do not present this entire image to the ANN for classification. Our goal is to identify features in the image that can be parameterized, and to compute much more concise parameter vectors from the image to submit to the net.

Note also that the CWT visualization makes the feature-selection process quite efficient. *Having developed a methodology on the gearbox data, we were able to construct low-dimensional feature sets for the two pump data sets in a matter of hours.*

2.3.3 Changing the Wavelet Basis

The two images in Plate B are from the first 500 msec of failed condensate pump data (CP-1A from Table 2-1). The left image is the analog of the smoothed helicopter CWT. It immediately shows the lack of stable, narrowband elements in the signal. Again, it would be imprudent to attempt classification based on the microstructure of the transient narrowband features in this image. Instead, we seek more broadband features.

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One appeal of the CWT is that it allows one to continuously vary time/scale resolution. By changing the wavelet on which the transform is based, one can sacrifice resolution in scale—which is exactly what is necessary to find broadband features. The right image is the same data, but using a wavelet transform with 1/10th the frequency resolution (along with additional smoothing over time to suppress transients and textures). This image clearly shows the locations of high energy content—and these regions are surprisingly stable compared to those of the left image.

2.3.4 Channel Selection

The two images in Plate C are from the first 500 msec of unfailed fire pump data (FP-3 from Table 2-2). The left image is from the radial channel, the right from the axial channel. Lines for the first few harmonics of the shaft rotation frequency (about 60 Hz) are clearly visible, along with a faint harmonic series based at about 400 Hz, and a broadband signal from 300 Hz to 1,500 Hz.

As mentioned earlier, we limited Phase I feature selection and failure detection/classification analysis to a single channel of data for each equipment type (so that we did not exhaust all of the potential processing gain on these clean data, and thus can offer ways to counter the additional complexity one would expect in field data). We selected the axial channel alone for further processing for the pump cases, and channel 5 alone for the gearbox case.

Since we had available another channel of helicopter gearbox data (channel 6, the only other data channel provided to us by NCCOSC), however, we decided to conduct a preliminary analysis of these data in order to explore the practical issues that must be confronted when dealing with more complicated vibrating systems where more than one channel of sensor data is available, either from the same location or from different locations. Recall that channels 5 and 6 come from accelerometers at the gearbox output end; channel 5 is oriented with the bearing load zone, and channel 6 is oriented orthogonal to this direction.

Using the same parameters and approach used for channel 5 data, we computed the CWTs from channel 6 data for each of the gearbox fault conditions. Discussion of the results are included in the two following subsections.

2.3.5 Gearbox Fault Signatures

Plate D shows segments of the CWT for the six cases of gearbox data. Each image represents 250 msec of signal, from 512 Hz to 16 kHz. Note the difference in structure of the CWT around the third harmonic of the mesh frequency (1,935 Hz)—both in breadth and texture.

Plate E shows a similar segment for channel 6 data. Note that the CWT features revealed by channel 6 data are not as sharply defined as those from channel 5; this is especially clear for the third harmonic on the normal case. The fifth harmonic (9,675 Hz) of the mesh frequency serves to separate the Inner Race and Rolling Element faults from the normal case. Also, the fourth harmonic appears to separate the five fault cases from the normal case as well.

The above findings show that by using features from both channel 5 and 6 a better distinction could be drawn among the six fault conditions. The best way to fuse these sources of information, however, was not addressed in the Phase I effort, but we plan to pursue this subject during Phase II.

2.3.6 Gearbox Fault Masks

Plate F shows the same segments of the CWT for the six cases of gearbox data, with low-energy regions masked out. Our rationale for this is to prevent using features that are weak, as they are easily compromised by disturbances or interference and hence do not contribute to high reliability detection. The technique used to mask these regions is a simple morphological filter applied across scale, masking areas that fall below an estimated noise floor. Note how this technique highlights the significant differences in structure around the third harmonic, and also of the 1,050 Hz line. Techniques such as this morphological filter provide quantitative insight into feature set performance before time and energy is spent training and testing an adaptive classifier.

Plate G shows a similar segment for channel 6. Note that the significant differences between channel 5 and channel 6 CWTs become clearer because of the masking of low-energy regions.

2.3.7 Condensate Pump Signatures

Plate H shows the CWTs for 125 msec of the axial channel for each of the eight condensate pump data segments in Table 2-1. The log frequency scale, between 16 Hz and 16 kHz, is divided into octaves. Segment 1 contains a fault of type 1, segments 3 and 8 each contain a fault of type 2, and the rest are good pumps (normal case). Note that the CWTs show clear differences between pumps in pairs of segments 1 and 2, 3 and 4, and 7 and 8. Each of these pairs includes a normal pump and a defective pump. On the other hand, segments 5 and 6, both from good pumps, display similar high-energy features.

In contrast with the helicopter gearbox data, the condensate pump CWTs contain wider high-energy regions, but they are—as in the gearbox case—relatively stable over time.

2.4 FEATURE SEPARATION

Detection and classification become exceptionally easy if the clusters of features corresponding to different cases exhibit two properties: convexity and separability. In these cases, classification becomes a matter of estimating boundaries to separate the clusters—and we can allocate one element of the hidden layer of an ANN to each cluster.

One never knows ahead of time whether or not a feature set will be convex and separable. We selected 500 msec of data from each test case as a basis for statistical analyses of separability. We used features that essentially correspond to a few frequency slices through the CWT—energies in particular frequency bands. We selected the set of bands to use on the basis of overall energy content—recall that robust classification is possible only from features with high energy differences between cases. In the cases of the gearbox and fire pump data, with strong, clear, narrow fundamentals, we adapted the frequencies to the center of that line (using the features themselves instead of referring to external synchronization signals). For the condensate pump data (which lack such a stable reference feature and whose energies are more dissipated across frequency), we left the frequency bands constant.

After collecting candidate features, but before training an ANN, we evaluated feature cluster separations. Table 2-3 shows the maximum separations between all pairs of clusters in

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terms of Fisher coefficients—essentially distances between cluster centers, normalized to units of standard deviations. This table was obtained by computing for each feature vector the Fisher coefficients between all fault condition pairs, and then selecting the maximum coefficient across all feature vectors for every fault condition pair. Any pair of clusters more than three or so units apart should be readily separable by an ANN classifier.

TABLE 2-3. PHASE I CLUSTER SEPARATIONS, HELICOPTER DATA

| | ND | IR | FE | OR | SP | TC |
|-----------------|-------|-------|-------|------|-------|-------|
| Normal | 0.00 | 5.67 | 10.79 | 9.79 | 11.14 | 11.28 |
| Inner Race | 5.67 | 0.00 | 4.13 | 5.25 | 13.31 | 6.05 |
| Rolling Element | 10.79 | 4.13 | 0.00 | 2.07 | 5.89 | 3.45 |
| Outer Race | 9.79 | 5.25 | 2.07 | 0.00 | 7.18 | 3.29 |
| Gear Spall | 11.14 | 13.31 | 5.89 | 7.18 | 0.00 | 8.61 |
| Tooth Cut | 11.28 | 6.05 | 3.45 | 3.29 | 8.61 | 0.00 |

We found that the CWT features provide good separation between cases. Below is a summary of the main characteristics of these features for each of the test systems.

Helicopter gearbox feature vectors (channel 5) contain heights of narrowband (1/35) octave lines

- center frequencies adapt to changes in fundamental mesh frequency
- lines were selected at the first six harmonics of mesh frequency, plus two other frequencies suggested by the CWT ($0.5525 * f$, $2.7 * f$, where f is the fundamental mesh frequency)
- feature clusters are nearly ellipsoidal
- minimum feature cluster separation is 2.07 Fisher units (standard deviations) (outer race/rolling element)

Condensate pump feature vectors (axial channel) contain energies in wider regions (1/6 octave)

- center frequencies are fixed over time (and cases)
- bands were selected at octave intervals (32 - 1,024 Hz), and at 1/4 octave intervals within high energy octaves (64 - 128 Hz, 512 - 1,024 Hz)

- feature clusters are nearly ellipsoidal
- minimum feature cluster separation is 5.87 Fisher units (CP-1A/CP-4B)

Fire pump feature vectors (axial channel) also contain both narrowband and broadband features

- center frequencies adapt to changes in fundamental shaft frequency (limited to within 2% nominal)
- narrow bands were selected at first 8 shaft harmonics, and at octave intervals within high broadband energy region (512 - 2,048 Hz)
- some feature clusters show some suspiciously high correlation (possibly due to clipping?)
- minimum feature cluster separation is 2.23 Fisher units (Fault 3/Fault 6)

The following three subsections graphically illustrate with color scattergrams the striking feature separation for some feature pairs and all fault conditions for each of the test systems examined in this work.

2.4.1 Gearbox Separation

Plate I presents the feature clusters computed from 3 seconds of gearbox data across all six cases. Feature vectors can be obtained every 10 msec, so there are about 300 sample vectors here. This plate shows the projection of the feature clusters onto a two-dimensional subspace defined by the power found in the second harmonic of the mesh frequency, and at a subharmonic line around 1,050 Hz. Note that: 1) all of the feature clusters appear convex, 2) the normal case is well separated from the fault cases by these two features alone, and 3) several pairs of faults can be separated as well. Other pairs of features provide different kinds of separation, but all show convex clusters.

2.4.2 Condensate Pump Separation

Plate J presents the feature clusters from 0.5 second of condensate pump data across all eight cases. There are about 30 feature vectors per case. It shows the projection of the feature clusters onto the two-dimensional subspace defined by the power near 615 Hz, and near 1,024 Hz.

Again, note that: 1) all of the feature clusters appear convex, 2) the normal cases are well separated from the fault cases by these two features alone, despite being more diffuse due to variations among units, and 3) type 1 and type 2 faults can be clearly separated as well. Other pairs of features provide different kinds of separation, but all show convex clusters.

2.4.3 Fire Pump Separation

Plate K presents the feature clusters computed from 0.5 second of fire pump data across all 16 cases. There are about 30 feature vectors per case. It shows the projection of the feature clusters onto the two-dimensional subspace defined by a narrow band around the seventh harmonic of the shaft rate and a wider band around 2,048 Hz. Note some suspicious characteristics of these clusters. The seventh harmonic of the normal data seems to be limited by a floor at 42 dB below the shaft fundamental, making detection and classification of fault type 3A (light blue squares) exceptionally easy. Also, for three of the test cases (one normal and two fault), the values of these features are exactly 6 dB apart, a relationship that is highly unlikely in truly random data. *It is important to supplement the power of data-driven approaches with some understanding of the physics of the system under study—why classification regions are the way they are—in order to gain confidence that the classification logic is truly robust to any artifacts that may be in the training data.*

2.4.4 Artifacts in Training Data

Through an example, this subsection illustrates the need to select features for classification based not only on their separation but also on the physics of the fault mechanism. The risk in not doing this is that data presented to the ANN classifier may contain variations upon which classification may be based, but which bear no causal relationship to fault mechanisms. For example, we selected a feature at the sixth harmonic of the mesh frequency for the gearbox data to serve as a disturbance detector. In this frequency range (12 kHz), there is very little energy in any of the data unless a disturbance is present. Our idea was that if a feature vector with relatively high energy (> 45 dB below the power in the mesh fundamental) were presented to the neural net, it would result in an ambiguous classification and any output deferred until the disturbance subsides.

Quite another thing happened. Plate L shows the gearbox feature clusters projected onto the subspace defined by the fifth and sixth harmonic power levels. Note the obvious separation between {Normal, Inner Race}, {Outer Race, Rolling Element, Tooth Cut}, and {Gear Spall}. The fact that the *magnitudes* of sixth harmonic power levels are so small suggests that this frequency is near a zero in the transfer function between the vibrating mechanics and the sensor. The fact that their *variation* is so small suggests that the energy in this band is largely background energy, or conveyed through a convoluted transmission path. In either case, *the variations among cases are unlikely to be caused by the faults themselves, but rather by the process of inserting and removing faults*. An adaptive classifier will happily use the power level at the sixth harmonic to separate the Normal case from, say, the Gear Spall. Only additional insight into the physics of the transmission mechanism, or a set of data including several insertions of the same fault, would prevent field deployment of a classifier that treats this insertion artifact as a valid source of information.

2.4.5 Guidelines for Finding Robust Feature Sets

Based on this Phase I effort we have developed a set of guidelines for finding robust feature sets in CWT images. These guidelines can be summarized as follows:

- Be sure that features *are robust to external disturbances*: we seek high energy content features to be derived from morphological filtering on the scale axis of the CWT, with narrow bandwidths to reduce their sensitivity to impulsive disturbances. Features must also be redundant to exploit the correlation among features, and they must be frequently computed as permitted by the largest time constant in the preprocessor.
- Be sure that features *are diverse*: it is desired to include features across a wide range of frequencies, for example, the first six harmonics of important narrowband vibrations (gearbox) or octave samples of broadband components (pumps). In addition, it is desired to include one or more low-energy features to support disturbance rejection.
- Be sure that features *distinguish normal from abnormal conditions*: for this we need to compute statistics (mean, standard deviation) on each CWT bin and look for significant differences that will lead to features with high discriminating power.

2.5 ARTIFICIAL NEURAL NETWORK CLASSIFIER

For an adaptive classifier we used a feedforward fully interconnected ANN of the back-propagation type with one input layer, one hidden layer, and one output layer. The number of processing elements (PEs) in the input layer varied with the vibrating system between 12 and 15. The number of output PEs also varied with the vibrating system, according to the number of fault conditions, including the normal cases. Because of the convexity and linear separation of the feature vector clusters for all the systems of Phase I, the number of hidden layer PEs was set equal to the number of output PEs. Table 2-4 presents the number of PEs per layer for each of these systems.

TABLE 2-4. NUMBER OF PROCESSING ELEMENTS PER ANN LAYER

| LAYER | HELICOPTER GEARBOX | CONDENSATE PUMPS | FIRE PUMPS |
|-----------|-----------------------|---------------------|------------|
| Input | 15 | 12 | 13 |
| Hidden | 6 | 8 | 16 |
| Output | 6 | 8 | 16 |
| Total PEs | 27 | 28 | 45 |

For the design, training, and testing of the ANNs we used a commercial software package, NeuralWorks (NeuralWare, 1992), running on a Macintosh platform. For each of the three systems, convergence to the specified RMS error of the difference between the desired and the actual outputs occurred relatively fast—after between 5,000 and 10,000 random presentations of the feature vectors included in the training set. *Given the simplicity of the ANNs used in this work, their small size, and the excellent feature clusters separation made possible by the judicious utilization of the CWT, no sophisticated training algorithms were required.*

From the test set results, we computed the following measures of effectiveness for each vibrating system: probability of false alarm, probability of missed detections, probability of misclassification, and probability of deferral. *Probability of false alarm* is the probability that a fault is announced when there is no fault present. *Probability of a missed detection* is the probability that no fault is announced when there is a fault present. *Probability of misclassification*

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is the probability that a fault type is announced when a different fault type is present. *Probability of deferral* is the probability that the classifier defers a decision when a case for decision (a feature vector) is presented to it.

For the purpose of this work, a feature vector leads to an ambiguous situation when the absolute difference between the two largest competing outputs is less than some specified tolerance. In these cases, the classifier refuses to announce a decision and considers the next feature vector. The consequence of this deferral is to decrease the probabilities of false alarm and missed detections, and to increase the time delay for a classifier decision. For instance, feature vectors for the gearbox system are computed every 10 msec, so the price paid in time delay for each deferral (or rejection) is 10 msec. delay in the time to detect a fault.

The statistical correlation between of feature vectors depends on the time constants embedded in the wavelet preprocessor designed to extract the selected feature set. Extracting feature vectors at a period exceeding the largest of these time constants leads to (approximate) statistical independence between successive feature samples. Since the ANN classification process is memoryless, this in turn assures (approximate) statistical independence between successive classifications. The period between feature reports can be quite short. Table 2-5 presents the maximum time constants and number of feature vectors per second allowed by such time constants for the three vibrating systems of Phase I.

TABLE 2-5. PREPROCESSOR TIME CONSTANTS AND FEATURE VECTOR RATES

| UNIT | MAX TIME CONSTANT | FEATURE VECTORS PER SECOND |
|--------------------|-------------------|----------------------------|
| Helicopter gearbox | 10 msec | 100 |
| Condensate pump | 25 msec | 40 |
| Fire pump | 25 msec | 40 |

We maintain statistical independence between successive feature vectors (i.e., compute them at a rate bounded below by the longest time constant in the preprocessor) precisely so that temporal fusion of classification results is simple. For the gearbox data, we computed feature vectors every 10 msec, and classified each and every one. To robustify the classification process against

transient disturbances, we can simply compare output classifications over a window of, say, 100 feature samples (one second of data). If, say, fewer than 95 of the classifications agree, we assume a disturbance (and not a fault) is present. This dramatically reduces the theoretical probability of false alarm, at the cost of an additional second of delay in producing a warning—a very attractive tradeoff for most situations.

2.6 FAULT DETECTION AND IDENTIFICATION RESULTS FROM PHASE I

Given the preceding insight into the derivation of high-energy wavelet features and the convex, separable clusters they form in feature space, it should be no surprise that good classification results are possible. *Providing a feature set that captures the important discriminants between normal operation and faults vastly simplifies the problem of designing an adaptive classifier that achieves good performance.*

The performance results for each of the test systems are presented in Table 2-6. The acceptance threshold is the ratio between the maximum output value and the next larger output value for a given feature vector. The complexity value is the total number of PEs in the corresponding ANN. For the gearbox and the condensate pumps systems, the test set was independent from the training set; for the fire pumps data these two sets were the same.

TABLE 2-6. PHASE I PERFORMANCE RESULTS

| | GEARBOX | CONDENSATE PUMP | FIRE PUMP |
|----------------------------------|---------|--------------------|-----------|
| TRAINING SET SIZE | 1125 | 240 | 480 |
| TEST SET SIZE | 6750 | 1400 | 4800 |
| ACCEPTANCE THRESHOLD | 1.4 | 1.2 | 2.0 |
| PROBABILITY OF FALSE ALARM | 0.000 | 0.000 | 0.000 |
| PROBABILITY OF MISSED DETECTION | 0.000 | 0.000 | 0.000 |
| PROBABILITY OF DEFERRAL | 0.035 | 0.020 | 0.020 |
| PROBABILITY OF MISCLASSIFICATION | 0.046 | 0.000 | 0.000 |
| COMPLEXITY | 27 PEs | 28 PEs | 45 PEs |

The performance results in Table 2-6 clearly show that *the wavelet feature sets selected above permit perfect detection performance with very low deferral rates.* While these results are

pleasing, we feel that an even more important principle has been demonstrated. *We used exactly the same method to find features for the pumps as we used for the gearbox data.* There was no trial and error for the pump classifiers—these results are from the very first feature sets we picked. This offers limited but important evidence that our results are not accidental—that *we have a methodology to analyze data from vibrating systems and derive small, focused feature sets that support high-confidence fault detection and classification.*

2.7 ANALYSIS OF FALSE ALARM AND DEFERRAL PROBABILITIES

The performance results in the previous subsection for the helicopter gearbox system are based on a test set containing 1,125 feature vectors for each of the fault conditions. To get greater insight into the detector's performance and the data presently available, we decided to compute performance measures for the normal case for a much longer test set (10 times longer) and to examine more closely the time histories of false alarms and deferrals and the tradeoff between these two measures. This subsection presents the results of this analysis. In particular, the insight gained through this analysis suggests additional means to improve the detector's performance, means which will be especially useful when dealing with helicopter gearboxes operating under more-severe environmental conditions.

2.7.1 Procedure

The longer test set for the gearbox normal case is the longest that can be extracted from the data available to us during Phase I. This data set contains 120 seconds of channel 5 vibrational readings sampled at 48 kHz. Since, as before, a feature vector is computed for every 512 samples, that is, every 10.67 msec, this data set provides 11,205 feature vectors for the normal case, after eliminating a small number of edge-effect contaminated feature vectors computed from the beginning of the data set. These feature vectors are then passed through the gearbox ANN classifier previously trained with 1,125 feature vectors *from all fault conditions*, including the normal case. This trained ANN is the same ANN used to obtain the performance results of the previous subsection.

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2.7.2 Gearbox False Alarm and Deferral Probabilities

The performance results for the longer testing set described above appear in Table 2-7. These results include only the false alarm and deferral probabilities for different acceptance thresholds for the helicopter gearbox system. Since this testing set contains only normal (or no-defect) case feature vectors, probabilities of missed detection and misclassification are not included in this table.

TABLE 2-7. FALSE ALARMS AND DEFERRALS FOR HELICOPTER GEARBOX

| Acceptance threshold | 0 | 5 | 6.7 | 10 |
|----------------------------|--------|--------|--------|--------|
| Probability of false alarm | 0.0159 | 0.0118 | 0.0116 | 0.0114 |
| Probability of deferral | 0 | 0.026 | 0.037 | 0.057 |

Table 2-7 shows that when no deferrals are allowed the probability of false alarm is relatively low (1.59%), and for a deferral probability (or deferral rate) as low as 4% the false alarm probability is 1.16%. These results are encouraging given that: 1) the testing set is 10 times longer than the entire training set, 2) the testing set includes "everything," that is, all the vibrational effects that were recorded during the entire 120 seconds of test bench operation, possibly including disturbances whose nature and duration were unknown to us, and 3) the trained ANN did not include a disturbance (or "strange effects") detector. (A well-designed and trained disturbance detector would be expected to drive down the false alarm probability by eliminating possible false alarm triggers.)

2.7.3 False Alarm Time History and Interarrival Times

Examination of the false alarm time history for a given deferral rate allows one to determine, for instance, whether false alarms occur in clusters or not, whether the false-alarm temporal distribution displays some regular pattern, and whether clusters, if any, are indicative of data characteristics unaccounted for by the training set. On the other hand, intercomparison of false alarm time histories for different deferral rates allows one to assess the tradeoff between false alarm and deferral probabilities.

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Figure 2-4 shows the false alarm time history for 0% deferral rate over the 11,205 epochs (approximately 120 seconds) at which feature vectors from the gearbox normal case were presented to the ANN classifier for a decision. The top part of the figure represents approximately the first 60 seconds, and the bottom part represents the last 60.¹ The number of false alarms for 0% deferral rate is 178. Figure 2-4 shows that when deferrals are not allowed, false alarms occur in two clusters on the left of the figure and rather randomly everywhere else. A discussion of this finding is presented later in this section.

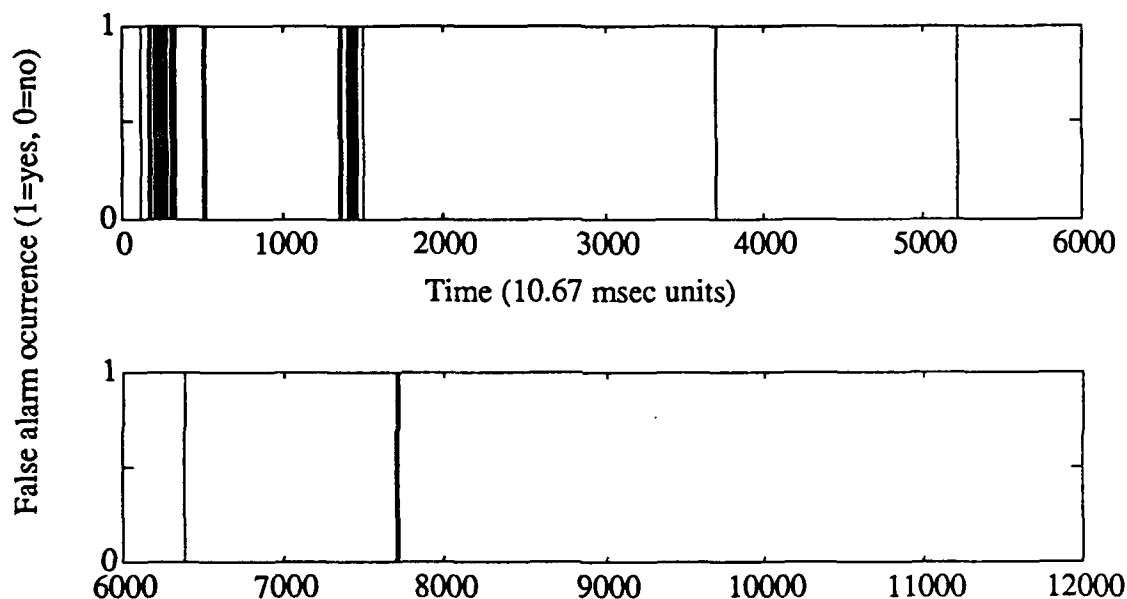


Figure 2-4. False Alarm Time History for 0% Deferral Rate

Histograms of the false alarm interarrival times appear in Fig. 2-5. Selected false-alarm interarrival-time statistics are presented in Table 2-8. Examination of the interarrival times shows that most of them are equal to 10.67 msec and come from the two clusters mentioned above.

¹ For this and subsequent time-history figures, note the following: To convert feature vector number to time in msec, the feature vector number must be increased by 20 (corresponding to the first 20 feature vectors discarded because of edge effects) and then multiplied by 10.67 msec, which is the time interval over which each feature vector is computed.

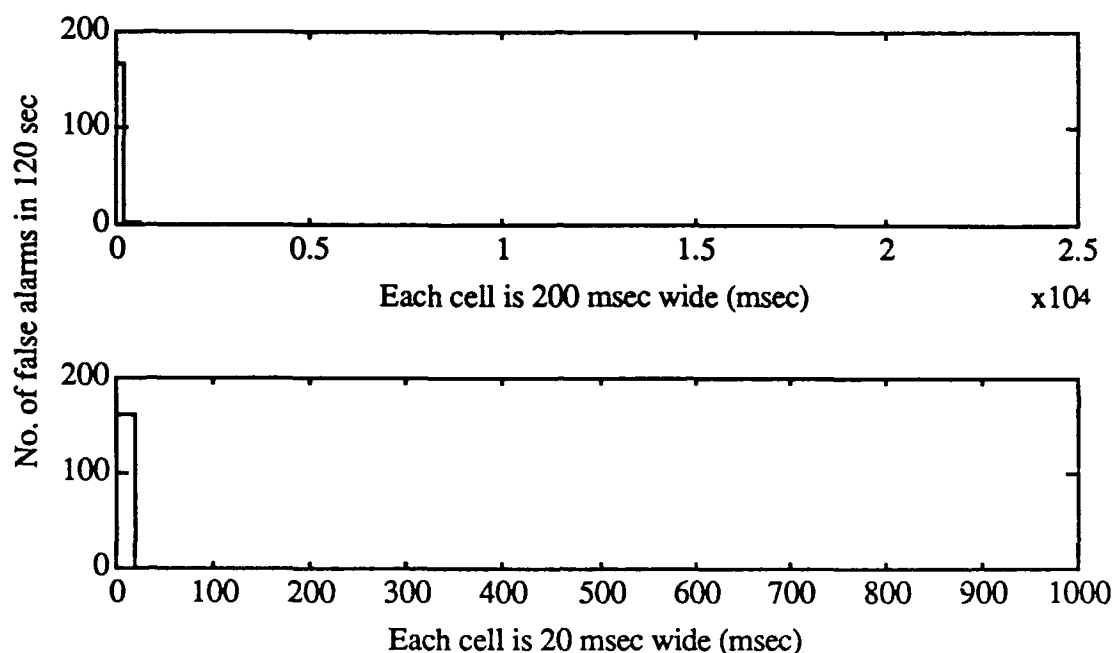


Figure 2-5. False-Alarm Interarrival-Times Histogram for 0% Deferral Rate

TABLE 2-8. FALSE-ALARM INTERARRIVAL-TIME STATISTICS FOR SEVERAL DEFERRAL RATES

| Deferral Rate | 0% | 3.7% | 5.7% |
|----------------------|---------|--------|-------|
| Minimum (msec) | 10.67 | 10.67 | 10.67 |
| Maximum (msec) | 23,573 | 138.67 | 85.33 |
| Mean (msec) | 457.22 | 12.90 | 12.01 |
| Std.Deviation (msec) | 2,625.7 | 13.76 | 9.16 |
| No. of false alarms | 178 | 125 | 120 |

The false-alarm time history for a 3.7% deferral rate is presented in Fig. 2-6. Note that by allowing the deferral rate to increase to a rather low value of 3.7%, the false alarms beyond the first cluster in Fig. 2-4 are eliminated; the number of false alarms for 3.7% deferral rate decreases to 125 (from 178 for a 0% rate).

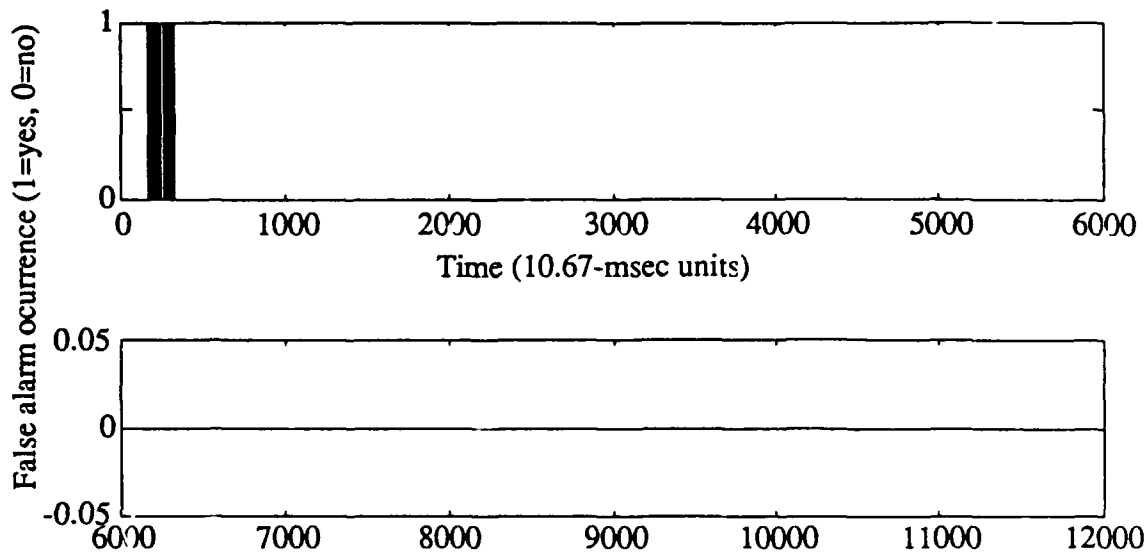


Figure 2-6. False-Alarm Time History for 3.7% Deferral Rate

The histogram of the corresponding false-alarm interarrival times is presented in Fig. 2-7. All of the false alarm interarrival times, except five, are equal to 10.67 msec. Selected statistics are presented in Table 2-8.

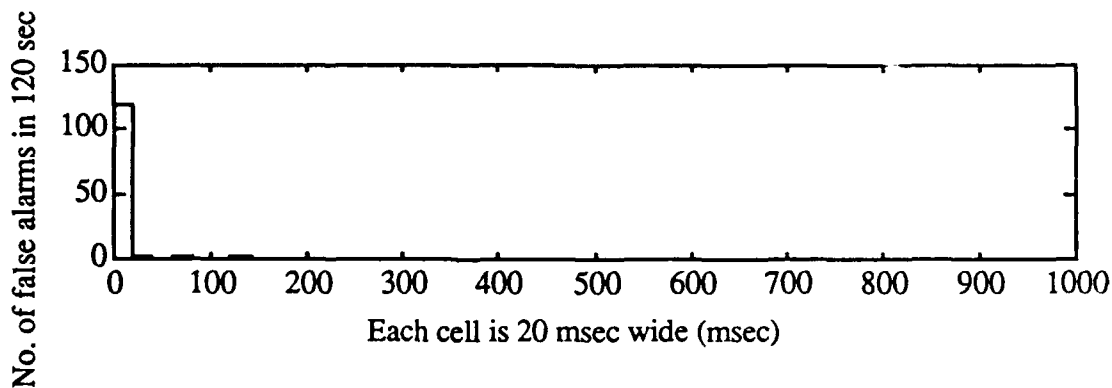


Figure 2-7. False-Alarm Interarrival-Time Histogram for 3.7% Deferral Rate

The false-alarm time history for a 5.7% deferral rate is presented in Fig. 2-8. Note that even after allowing the deferral rate to further increase to a value of 5.7%, most of the false alarms in the first cluster in Fig. 2-6 still remain; in fact, the number of false alarms for a 5.7% deferral rate only decreases to 120 (from 125 for a 3.7% rate). All of the corresponding false-alarm interarrival times, except three, are equal to 10.67 msec. Selected statistics are presented in Table 2-8.

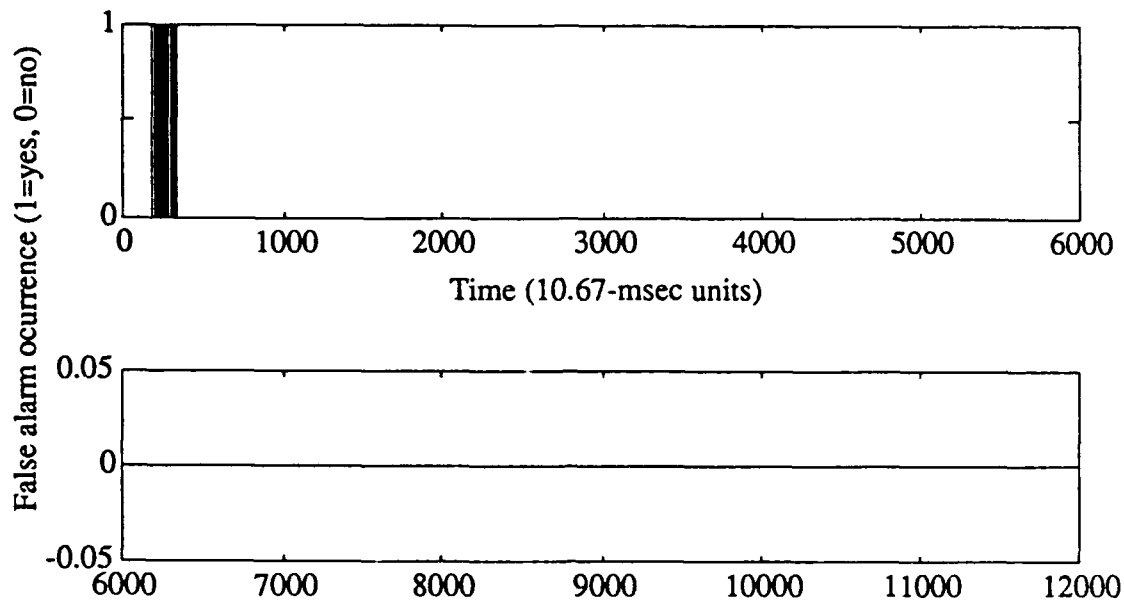


Figure 2-8. False-Alarm Time History for 5.7% Deferral Rate

The above finding—the persistence of the false alarm cluster in Fig. 2-8 even after allowing the deferral rate to increase to 5.7% —suggests that some unknown disturbance occurred at that time interval, approximately between the 2nd and the 3rd second of the data set. Therefore, we examined the first 4 seconds of the data set in great detail.

Figure 2-9 displays the accelerometer readings for the first 4 seconds of channel 5 of the helicopter gearbox normal case. Note that starting at about 2.0 sec from the beginning of the record a disturbance (unknown to us) starts to develop until about 2.7 sec, and from this point on until 3.6 sec the signal drops out to zero.

In Fig. 2-8, comparing the time interval where the false alarm cluster occurs (between 1.9 and 3.5 sec) and the time interval where the unknown disturbance occurs immediately reveals why the false alarm cluster does not go away even when the deferral rate is allowed to increase from 0% to 5.7%. More importantly, this correspondence between a disturbance and a false alarm cluster clearly suggests that if we had included a well-trained disturbance detector in our ANN classifier, the false alarm probabilities would have been much more lower!

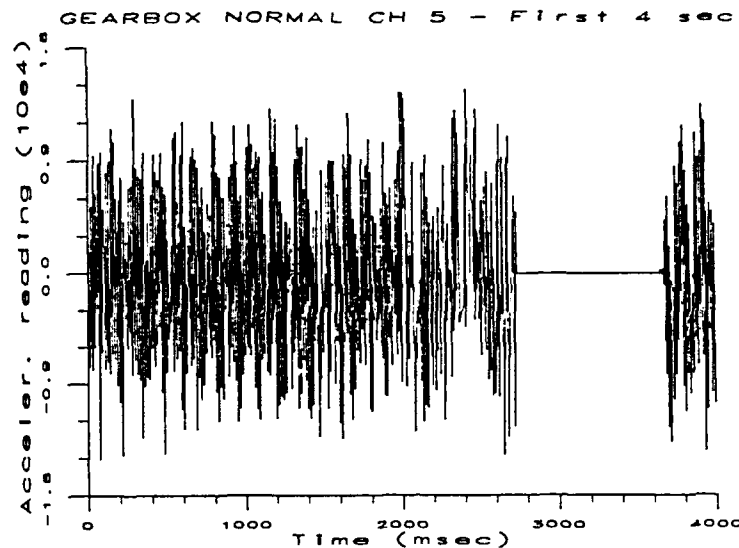


Figure 2-9. Accelerometer Readings for First 4 Seconds of Channel 5—Normal Case

The above finding has important practical implications for the work that we plan to conduct during Phase II of this effort. Since helicopter gearboxes operating under more severe environmental conditions are subject to many kinds of disturbances, the above finding suggests that detection performance under real-world conditions could be improved significantly if a disturbance detector is added to the ANN classifier. Also, adding to the detector the capability to monitor the false alarm time history for the presence of clusters to make it self-monitoring will additionally improve its performance.

2.7.4 Deferral Time History and Interarrival Times

The analysis of the deferral time history complements the corresponding analysis of false alarms. By analyzing the deferral time history one can determine, for instance, whether deferrals occur in clusters or more sparsely distributed, and whether a given deferral rate causes an unacceptable delay temporal distribution for a given false alarm probability. As discussed previously, the price paid for every deferral is a delay equal to the time interval for which a feature vector is computed; for the gearbox system every deferral introduces a delay of 10.67 msec in the classifier's announcement of a classification decision.

The deferral time history for a deferral rate of 3.7% is displayed in Fig. 2-10. This deferral rate corresponds to a false alarm probability of 1.16%. Note the presence of a deferral cluster on

about the same time interval where a disturbance-caused false alarm is present in Fig. 2-4. This suggests again that if a disturbance detector is included in the ANN classifier, both the number of false alarms and the number of deferrals should decrease, an effect which obviously contributes to overall performance improvement of the classifier.

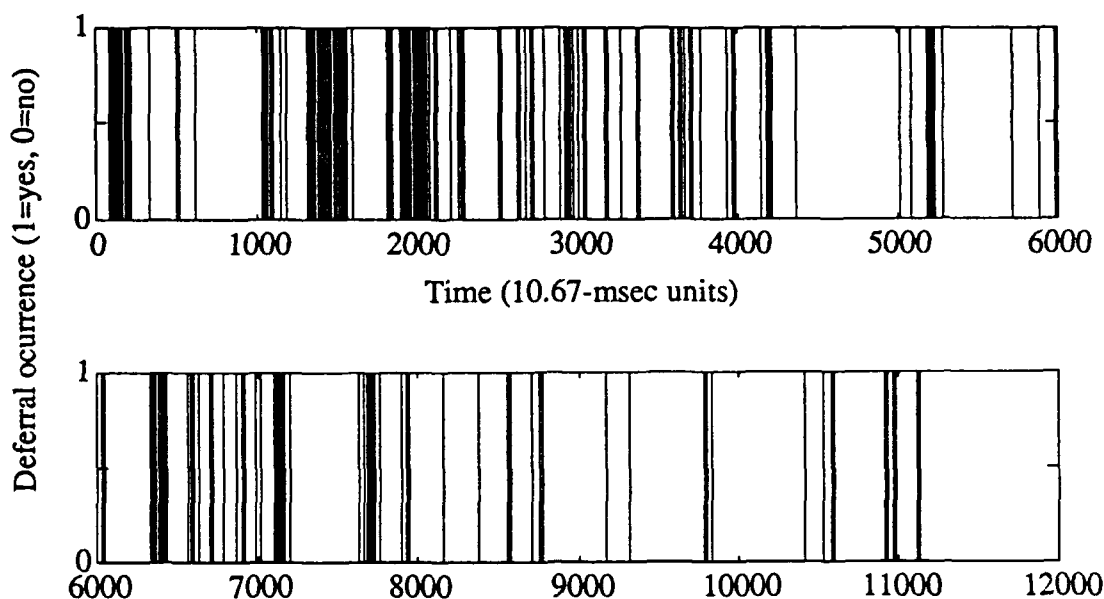


Figure 2-10. Deferral Time History for 3.7% Deferral Rate

Figure 2-11 displays the deferral time history for a 5.7% deferral rate, which corresponds to a false alarm probability of 1.14%. Note that as the number of deferrals increases, as it should, the number of deferral clusters does not increase significantly, which indicates that the increase from 3.7% to 5.7% in the deferral rate does not result in significant additional concentrated time delays in the sequence of classifier decisions. Selected statistics for deferral interarrival times for deferral rates of 3.7% and 5.7% are included in Table 2-9.

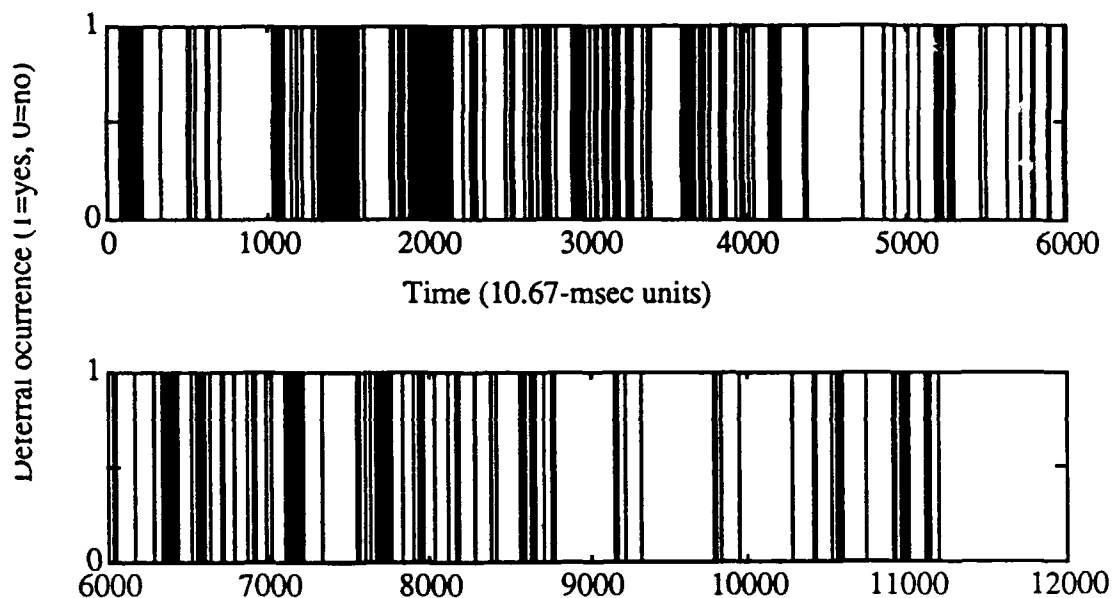


Figure 2-11. Deferrals Time History for 5.7% Deferral Rate

TABLE 2-9. DEFERRAL INTERARRIVAL-TIME STATISTICS

| Deferral Rate | 3.7% | 5.7% |
|----------------------|--------|--------|
| Minimum (msec) | 10.67 | 10.67 |
| Maximum (msec) | 6,901 | 4,992 |
| Mean (msec) | 288.18 | 185.6 |
| Std Deviation (msec) | 797.31 | 467.32 |
| No. of deferrals | 410 | 640 |

SECTION 3

CONCLUSIONS AND RECOMMENDATIONS

3.1 CONCLUSIONS FROM THE PHASE I EFFORT

Our Phase I performance results speak for themselves. *Incipient fault detection and classification on bench-test and mild-operation data is quite feasible*, even without exploiting many additional techniques available. The CWT provides images from which feature selection is easy. These features are simple and robust (high energy, narrow bandwidth).

There are no technological impediments to practical implementation. The selected wavelet features can be computed using off-the-shelf digital filtering hardware. ANNs can be trained and employed using off-the-shelf techniques.

The helicopter gearbox data used was bench test data. Bench test data cannot support a complete characterization of normal operating regimes and cannot include a complete set of disturbances to be encountered in the field. Moreover, seeded fault data cannot span the complete set of possible failures, and may contain artifacts that assist detection. In summary, *bench tests are not reality*. Reality is much less controlled, and hence much less predictable. Although the pump data were obtained under actual operating conditions, these conditions were relatively benign and do not include all possible operating conditions. Therefore, the principal conclusion we draw from Phase I is to greet these results (or any Phase I results) with skepticism concerning their applicability to field systems, and that *any Phase II effort must focus on support for analysis and design with real data* under widely varied operating regimes.

We are well positioned to make the transition to real data in Phase II because of the methodology we established in Phase I. *We have a specific procedure for selecting low-dimensional, robust feature sets*—and have demonstrated its efficacy on the two pump data sets.

We deliberately avoided using all available processing techniques to solve the Phase I problem—we wanted to be sure that a simple problem could be solved with simple techniques. We arbitrarily limited ourselves to single-channel processing, with instantaneous classification. *This makes available substantial additional processing power to meet the challenges posed by using real data, and we recommend exploiting it to the fullest in Phase II.*

3.2 PHASE II RECOMMENDATIONS

Phase I demonstrated the feasibility of achieving good fault detection and classification performance based on a single channel of accelerometer data for each of the three vibrating systems studied in this effort. Preliminary analysis of the helicopter gearbox data from a different channel (channel 6) showed that there is indeed additional information in other channels that could be profitably used to improve the ANN classifier's performance. Analysis of false alarm time histories for the helicopter gearbox indicated that to drive down the false alarm probability is necessary to characterize as much as possible the normal behavior of the vibrating system, including all possible kinds of disturbances. This characterization will require the analysis of vibrational data from systems operating under the broadest possible range of environmental conditions.

The major output of Phase I is a methodology for failure detection and identification from accelerometer data that can be applied to any vibrating system having the characteristics of the systems included in this effort. This methodology has been successfully demonstrated for test bench data and mild-operation data. To convert this methodology into a practical and useful tool for real vibrating systems is indispensable to test it with real-world data from systems operating under more severe environmental conditions. Therefore, Phase II must concentrate on this task, and its successful performance will depend critically on the availability of this type of data.

Information obtained during the course of this Phase I effort indicates that a government agency (NCCOSC/NRaD) will soon collect extensive amounts of seeded fault data and unfailed flight data for helicopter gearboxes, which will be available to researchers involved in failure detection and identification. Extensive helicopter gearbox data might be obtained in principle from helicopter manufacturers such as Boeing or Sikorsky, with whom we have already held

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preliminary technical interchanges. Given this projected availability of helicopter data, the need of Phase II to focus on real-world data, and DARPA's continuing interest on high-payoff applications, we will base the recommendations to be presented next on the assumption that *the Phase II effort will concentrate exclusively on incipient detection and identification of helicopter gearbox failures.*

The major output of Phase II must be a preliminary design of a hardware/software system for real-time incipient detection of helicopter gearbox failures under operational conditions. This design will be determined by timing, sizing, and other implementation tradeoffs determined in turn by the outcome of additional research and development to be conducted during Phase II.

The main issues to be addressed in Phase II include: 1) use of multichannel data, particularly for separating airframe vibrations from internal gearbox vibrations, 2) use of situational data which characterizes the different environmental conditions under which helicopters operate to schedule the classification weights (and perhaps even the feature set) as conditions change, 3) clarification of the maintenance concept for helicopter gearboxes (e.g., when does ANN training take place?), and 4) selection of the best technology for Phase III implementation. We discuss these topics in more detail below.

Use of multichannel data: One is not limited to single-channel accelerometer data in many potential applications. Some issues to be addressed include: How can one process additional channels? Is there advantage to using a *vector* wavelet transform to process all channels simultaneously? What can wavelet phase information, neglected in this effort, contribute to separating internal and external sources of vibration? Can statistical techniques derived for use in wavelet transform space be adapted to vector transforms? Is there a need for different techniques on different channels? To what extent can accelerometers mounted on the supports of a vibrating system, rather than on its casing, supply information about environmental vibrations and disturbances? How should this information influence the feature-selection process?

Use of situational data: We believe that the most practical approach to incipient failure detection is to characterize as much as possible all manifestations of gearbox normal behavior. If

this characterization is successful, for any given situation the classifier will be able to detect any failure condition. One key advantage of this approach is that in principle it only requires unfailed data, which is easier and safer to collect than seeded or unseeded fault data. On the other hand, this approach requires the collection of situational data, that is, data representing the most important environmental conditions under which the helicopter operates. This type of data includes, for instance, altitude, speed, weather data, load, maneuvers being conducted, commanded engine torque, and kinematic acceleration. Situational data could be used as parameters to characterize the different regions of normal behavior. Issues to be addressed include: Which group of situational variables provide a satisfactory delimitation of different normal operating regimes? Which elements should be included in a software capability to allow the effective use of situational data for detection of abnormal conditions? Is it better to use situational variables to parameterize different classifiers or to include situational variables as inputs to a more general classifier?

Clarification of the maintenance concept: There are several issues related to incorporating incipient failure detectors into a genuine helicopter gearbox maintenance concept. Is the ANN trained for a specific platform, or for an entire class? Is it retrained after major overhauls? What are the relative merits of detection alone vs. detection and classification? What are acceptable false alarm rates? Are there other meaningful outputs from an incipient fault detector (e.g., rate of development of an anomaly) that can be useful to an operator? And, of course, what response time is required, and how can that time be used to process a series of feature vectors in order to reduce false alarms and increase detection reliability?

Selection of implementation technology: The Phase I effort yielded a preprocessor/classifier design that, while evaluated using non-real-time software emulations, can be readily implemented in hardware for real-time operation. We anticipate the Phase II enhancements will yield equally simple real-time computation requirements. To preserve the possibility of immediate Phase III application, Phase II should resolve the basic hardware design issues for the real-time element. What is the overall complexity of the processing? If implemented digitally, what throughput is needed (counted as fixed-point multiplies per second), and what opportunities for

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parallelism or pipelining exist? If implemented in analog circuitry, what component tolerances are necessary? If implemented as a mix of digital and analog elements, what is the best role for each?

There are some other technical areas that would benefit from additional research attention: Can one perform the statistical evaluation of wavelet features directly in wavelet-transform space (i.e., for all candidate features) rather than for selected features in a post-transform analysis? Can one apply advanced multiscale estimation techniques to extract different features at different time scales? How effective might be some additional wavelet feature types (e.g., wavelet packet coefficients for switching systems, or multiscale autoregressive model identification)? Can recent work on the interpretation of ANN outputs as likelihood functions be directly linked to the statistical performance analysis currently done in feature space?

In summary, we recommend that the central objective of Phase II be to deliver a *preliminary design of a hardware/software system* for real-time detection of helicopter gearbox failures under real-world operating conditions. This design will include the capability to use *multichannel sensor data* and *situational data*, and its performance will be measured according to the requirements of a *clear maintenance concept* prepared during Phase II. Phase II also should be used to plan for and gather information about the resources required for a successful implementation in Phase III of the technology developed in the two previous phases.

REFERENCES

- Basseville, M., "Detecting Changes in Signals and Systems—A Survey," *Automatica*, Vol. 24, 1987, pp. 309-326.
- Coifman, R.R. and M.V. Wickerhauser, "Entropy-Based Algorithms for Best Basis Selection," *IEEE Trans. Inform. Theory*, Vol. 38, No. 2, March 1992, pp. 713-718.
- Coifman, R.R., Y. Meyer, S. Quake, and M.V. Wickerhauser, "Signal Processing and Compression with Wave Packets," preprint, April 1990.
- Daubechies, I., "The Wavelet Transform, Time-Frequency Localization and Signal Analysis," *IEEE Trans. Inform. Theory*, Vol. 36, 1990, pp. 961-1005.
- Grossman, A., R. Kronland-Martinet, and J. Morlet, "Reading and Understanding Continuous Wavelet Transforms", in *Wavelets, Time-Frequency Methods and Phase Space*, J.M. Combes, A. Grossman, and Ph. Tchamitchian (Eds.), Springer-Verlag, 1989.
- KHOROS Group, "Khoros Software," Department of Electrical and Computer Engineering, University of New Mexico, Albuquerque, NM, 1992.
- Kronland-Martinet, R., J. Morlet, and A. Grossman, "Analysis of Sound Patterns Through Wavelet Transforms", *Int. Journal of Pattern Recognition and Artificial Intelligence*, Vol. 1, No. 2, 1987, pp. 273-302.
- Lau, C. and B. Widrow, Special Issue on Neural Networks, I: Theory and Modeling, *Proc. IEEE*, September 1990.
- Lau, C. and B. Widrow, Special Issue on Neural Networks, II: Analysis, Techniques, and Applications, *Proc. IEEE*, October 1990.
- Mallat, S.G., "A Theory for Multiresolution Signal Decomposition: The Wavelet Representation," *IEEE Trans. Pattern Anal. Machine Intell.*, Vol. 11, July 1989, pp. 674-693.
- Mallat, S.G., "Multifrequency Channel Decompositions of Images and Wavelet Models," *IEEE Trans. Acoust., Speech, Signal Processing*, Vol. 37, December 1989, pp. 2091-2110.
- Meyer, Y., *Ondelettes et Operateurs*, Hermann, 1988.
- NeuralWare, Inc., "NeuralWorks Professional II/PLUS Software", Pittsburgh, PA, 1992.
- Ruskai, M.B., G. Beylkin, et al., (Eds), *Wavelets and Their Applications*, Jones and Bartlett Publishers, Boston, 1992.
- Vetterli, M. and C. Herley, "Wavelets and Filter Banks: Relationships and New Results," *Proc. ICASSP*, Albuquerque, NM, 1990.
- Weiss, J.L., and J.Y. Hsu, "Integrated Restructurable Flight Control Demonstration Results," NASA CR-178305, NASA Langley Research Center, May 1987.
- Widrow, B., R. Winter, and R. Baxter, "Layered Neural Nets for Pattern Recognition," *IEEE Trans. Acoust., Speech, Signal Processing*, Vol. 36, 1988, pp. 1109-1118.
- Willsky, A.S., "A Survey of Design Methods for Failure Detection in Dynamic Systems," *Automatica*, November 1976, pp. 601-611; also presented as an invited paper at the MIT, NASA-Ames Workshop on System Reliability for Future Aircraft, Cambridge, MA, August 1975 (NASA Report NASA CP-003); also in AGARDograph No. 224 on Integrity in Electronic Flight Control Systems.

ADDITIONAL RELEVANT PUBLICATIONS BY PHASE I TEAM MEMBERS

- Basseville, M. A. Benveniste, A.S. Willsky, and K.C. Chou, "Multiscale Statistical Processing," *Proc. Int. Symp. Math. Theory of Networks Syst.*, Amsterdam, June 1989.
- Basseville, M., A. Benveniste, and A.S. Willsky, "Multiscale Autoregressive Processes, Parts I and II," *IEEE Trans. Signal Processing*, August 1992.
- Basseville, M., A. Benveniste, K.C. Chou, S.A. Golden, R. Nikoukhah, and A.S. Willsky, "Modeling and Estimation of Multiresolution Stochastic Processes," *IEEE Trans. Inform. Theory*, Vol. 38, No. 2, March 1992, pp.766-784.
- Chou, K.C. A.S. Willsky, A. Benveniste, and M. Basseville, "Recursive and Iterative Estimation Algorithms for Multi-Resolution Stochastic Processes," *Proc. 28th IEEE Conf. Decision Contr.*, Tampa, FL, December 1989.
- Chou, K.C. and A.S. Willsky, "Multiscale Riccati Equations and a Two-Sweep Algorithm for the Optimal Fusion of Multiresolution Data," *Proc. 29th IEEE Conf. Decision Contr.*, Honolulu, HI, December 1990.
- Chou, K.C., S. Golden, and A.S. Willsky, "Modeling and Estimation of Multiscale Stochastic Processes," *ICASSP-91*, Toronto, April 1981.
- Chow, E.Y. and A.S. Willsky, "Analytical Redundancy and the Design of Robust Failure Detection Systems," *IEEE Trans. Automat. Contr.*, Vol. 29, July 1984, pp. 603-604.
- Chow, E.Y. and A.S. Willsky, "Bayesian Design of Decision and Rules for Failure Detection," *IEEE Trans. Aerospace and Electronic Syst.*, Vol. 20, No. 6, November 1984, pp. 761-774.
- Chow, E.Y., X.-C. Lou, G.C. Verghese, and A.S. Willsky, "Redundancy Relations and Robust Failure Detection," in *Detection of Abrupt Changes in Signals and Dynamical Systems*, M. Basseville and A. Benveniste (Eds.), Springer-Verlag Lecture Notes in Control and Information Sciences, No. 77, 1986.
- Deckert, J.C., M.N. Desai, J.J. Deyst, and A.S. Willsky, "F8-DFBW Sensor Failure Identification Using Analytic Redundancy," *IEEE Trans. Automat. Contr.*, Vol. AC-22, No. 5, October 1977, pp. 795-803.
- Dowdle, J.R., M. Athans, S. Gully, and A.S. Willsky, "Optimal Estimation of Maneuvering Targets for Missile End-Game Guidance," *Proc. Amer. Contr. Conf.*, Arlington, VA, June 1982.
- Eterno, J.S., J.L. Weiss, D.P. Looze, and A.S. Willsky, "Design Issues for Fault Tolerant- Restructurable Aircraft Control," *IEEE Conf. Decision Contr.*, December 1985.
- Grunberg, D.B., J.L. Weiss, and J.C. Deckert, "Generation of Optimal and Suboptimal Strategies for Multiple-Fault Isolation," *Proc. IEEE Int'l. Automatic Testing Conf.*, San Francisco, CA, 3-5 November 1987, pp. 125-131.
- Grunberg, D.B., P. Kapasouris, J.L. Weiss, J.C. and Deckert, "Computer-Aided Design Techniques for Test System Development: Phase II Final Report," TR-418, ALPHATECH, Inc., Burlington, MA, January 1989.

ALPHATECH, INC.

- Gustafson, D.E., A.S. Willsky, J.-Y. Wang, M.C. Lancaster, and J.H. Triebwasser, "A Statistical Approach to Rhythm Diagnosis in Cardiograms," *Proc. IEEE*, Vol. 65, No. 5, May 1977, pp. 802-804.
- Gustafson, D.E., A.S. Willsky, J.-Y. Wang, M.C. Lancaster, and J.H. Triebwasser, "ECG/VCG Rhythm Diagnosis Using Statistical Signal Analysis I: Identification of Persistent Rhythms," *IEEE Trans. Biomed. Eng.*, Vol. 25, July 1978, pp. 344-353.
- Gustafson, D.E., A.S. Willsky, J.-Y. Wang, M.C. Lancaster, and J.H. Triebwasser, "ECG/VCG Rhythm Diagnosis Using Statistical Signal Analysis II: Identification of Transient Rhythms," *IEEE Trans. Biomed. Eng.*, Vol. 25, July 1978, pp. 353-361.
- Korn, J., S. Gully, and A.S. Willsky, "Tracking of Maneuvering Aircraft by Surface-to-Air Missiles," *Proc. Amer. Contr. Conf.*, Arlington, VA, June 1982.
- Lou, X.-C., A.S. Willsky, and G.C. Verghese, "Optimally Robust Redundancy Relations for Failure Detection in Uncertain Systems," *Automatica*, Vol. 22, 1986, pp. 333-344.
- Mier-Muth, A.M. and A.S. Willsky, "A Sequential Method for Spline Approximation with Variable Knots," *Int. J. of System Science*, Vol. 9, September 1978, pp. 1055-1067.
- Pattipati, K.R., A.S. Willsky, J.C. Deckert, J.S. Eterno, and J.L. Weiss, "A Design Methodology for Robust Failure Detection and Isolation," *Proc. Amer. Contr. Conf.*, San Diego, CA, 6-8 June 1984, pp. 1755-1762.
- Pattipati, K.R., Alexandridis, M.G., and Deckert, J.C., "Efficient Sequencing of Diagnostic Tests," *Proc. 40th Meeting of the Mechanical Failures Prevention Group*, National Bureau of Standards, Gaithersburg, Maryland, 16-18 April 1985, pp. 122-135.
- Pattipati, K.R., J.C. Deckert, and M.G. Alexandridis, "Time-Efficient Sequencer of Tests (TEST)," *Proc. IEEE Int. Automatic Testing Conf.*, Uniondale, NY, 22-24 October 1985, pp. 49-62.
- Pattipati, K.R., J.J. Shaw, J.C. Deckert, L.K. Beean, M.G. Alexandridis, and W.E. Lougee, "CONFIDANTE: A Computer-Based Design Aid for the Optimal Synthesis, Analysis, and Operation of Maintenance Facilities," *Proc. IEEE Automatic Testing Conf.*, Washington, DC, 5-7 November 1984, pp. 390-404.
- Pattipati, K.R., M.G. Alexandridis, and J.C. Deckert, "A Heuristic Search/Information Theory Approach to Near-Optimal Diagnostic Test Sequencing," *Proc. IEEE Int. Conf. Syst., Man, Cybern.*, Atlanta, GA, 14-17 October 1986, pp. 230-235.
- Weiss, J.L., A.S. Willsky, D.P. Looze, J.T. Crawford, and R.R. Huber, "Detection and Isolation of Control Surface Effectiveness Failures in High-Performance Aircraft," *Proc. National Aerospace and Electronics Conf.*, Dayton, OH, May 1985.
- Weiss, J.L., A.S. Willsky, K.R. Pattipati, and J.S. Eterno, "Application of FDI Metrics to Detection and Isolation of Sensor Failures in Turbine Engines," *Proc. Amer. Contr. Conf.*, Boston, MA, June 1985, pp. 1114-1120.
- Weiss, J.L., J.C. Deckert, and K.B. Kelly, "Analysis and Demonstration of Diagnostic Performance in Modern Electronic Systems," RL-TR-91-180, Rome Laboratory, Griffiss AFB, NY, August 1991.
- Weiss, J.L., K.R. Pattipati, A.S. Willsky, J.S. Eterno, and J.T. Crawford, "Robust Detection/Isolation/Accommodation for Sensor Failures," ALPHATECH Technical Report TR-213, September 1984.
- Weiss, J.L., K.R. Pattipati, A.S. Willsky, J.S. Eterno, and J.T. Crawford, "Robust Detection/Isolation/Accommodation for Sensor Failures," NASA CR-174797, NASA Lewis Research Center, September 1985.

ALPHATECH, INC.

- Weiss, J.L., M. Doyle-Buckley, and J.C. Deckert, "A Prototype Test-Engineering Workstation," Proc. National Aerospace and Electronics Conf., Dayton, OH, June 1989, pp. 1937-1943.
- Willsky, A.S. and H.L. Jones, "A Generalized Likelihood Ratio Approach to the Detection and Estimation of Jumps in Linear Systems," *IEEE Trans. Automat. Contr.*, Vol. AC-21, February 1986, pp. 108-112.
- Willsky, A.S., "Detection of Abrupt Changes in Dynamic Systems," in *Detection of Abrupt Changes in Signals and Dynamical Systems*, M. Basseville and A. Benveniste (Eds.), Springer-Verlag Lec. Notes in Control and Information Sciences, No. 77, 1986.
- Willsky, A.S., "Multiscale Stochastic Processes and Wavelet Transforms," *Lowell Conference on Wavelets*, Lowell, MA, June 1990, invited presentation.
- Willsky, A.S., E.Y. Chow, S.B. Gershwin, C.S. Greene, P.K. Houpt, and A.L. Kurkjian, "Dynamic Model-Based Techniques for the Detection of Incidents on Freeways," *IEEE Trans. Automat. Contr.*, Vol. AC-25, No. 3, June 1980, pp. 347-360.
- Willsky, A.S., J.J. Deyst, and B.S. Crawford, "Two Self-Test Methods Applied to an Inertial System Problem," *AIAA J. Spacecraft and Rockets*, Vol. 12, July 1975, pp. 434-437.

SELECTED BIBLIOGRAPHY ON FAULT DETECTION/ISOLATION AND

WAVELETS

- Basseville, M. and A. Benveniste, "Sequential Detection of Abrupt Changes in Spectral Characteristics of Digital Signals," *IEEE Trans. Inform. Theory*, Vol. 29, September 1983, pp. 709-723.
- Basseville, M., A. Benveniste, and G. Moustakides, "Detection and Diagnosis of Abrupt Changes in Modal Characteristics of Nonstationary Digital Signals," *IEEE Trans. Inform. Theory*, Vol. 32, May 1986, pp. 412-417.
- Basseville, M., A. Benveniste, G. Moustakides, and A. Rougee, "Detection and Diagnosis of Changes in Eigenstructure of Nonstationary Multivariable Systems," *Automatica*, Vol. 23, 1987, pp. 479-489.
- Benveniste, A. and J.-J. Fuchs, "Signal Sample Modal Identification of a Nonstationary Stochastic Process," *IEEE Trans. Automat. Contr.*, Vol. 30, January 1985, pp. 66-74.
- Benveniste, A., M. Basseville, and G. Moustakides, "The Asymptotic Local Approach to Change Detection and Model Validation," *IEEE Trans. Automat. Contr.*, Vol. 32, 1987, pp. 583-592.
- Beylkin, G., R. Coifman, and V. Rokhlin, "Fast Wavelet Transforms and Numerical Algorithms I," *Commun. Pure and Appl. Math.*
- Burt, P.J. and E.H. Adelson, "The Laplacian Pyramid as a Compact Image Code," *IEEE Trans. Commun.*, Vol. 30, No. 4, April 1983, pp. 532-540.
- Cheung, J. and G. Stephanopoulos, "Representation of Process Trends—Part I: A Formal Representation Framework," *Computers Chem. Eng.*, Vol. 14, No. 4/5, 1990, pp. 495-510.
- Cheung, J. and G. Stephanopoulos, "Representation of Process Trends—Part II: The Problem of Scale and Qualitative Scaling," *Computers Chem. Eng.*, Vol. 14, No. 4/5, 1990, pp. 511-539.
- Chou, K.C., "A Stochastic Modeling Approach to Multiscale Signal Processing," PhD Thesis, MIT, May 1991.
- Daubechies, I., "Orthonormal Bases of Compactly Supported Wavelets," *Commun. Pure and Appl. Math.*, Vol. 41, November 1988, pp. 909-996.
- Desai, M. and D.J. Shazeer, "Acoustic Transient Analysis Using Wavelet Decomposition," *Neural Networks for Ocean Engineering Workshop*, Washington, DC, August 1991.
- Doyle-Buckley, M. and J.L. Weiss, "ALPHATECH Program for Testability (APT) Computing Environment (ACE)," TR-362-2, ALPHATECH, Inc., Burlington, MA, January 1989.
- Frank, P.M., "Fault Diagnosis in Dynamic System via State Estimation—A Survey," in Tzafestas et al. (Eds.), *Reliability and Related-Knowledge-Based Approaches*, Vol. 1, 1987, pp. 35-98, D. Reidel Publishing Company.
- Friedlander, B. and B. Porat, "Detection of Transients by the Gabor Representation," *IEEE Trans. Acoust., Speech, Signal Processing*, Vol. 37, February 1989, pp. 169-180.

ALPHATECH, INC.

- Friedlander, B. and B. Porat, "Performance Analysis of Transient Detectors Based on a Class of Linear Data Transforms," *IEEE Trans. Inform. Theory*, Vol. 38, No. 2, March 1992, pp. 665-673.
- Frisch, M. and H. Messer, "Detection of a Transient Signal of Unknown Scaling and Arrival Time Using the Discrete Wavelet Transform," *ICASSP-91*.
- Glowinski, R., W. Lawton, M. Ravachol, E. Tennenbakum, "Wavelet Solution of Linear and Nonlinear Elliptic, Parabolic, and Hyperbolic Problems in One Space Dimension," *9th SIAM Int. Conf. Comp. Methods in Appl. Sci. and Eng.*, 1990.
- Golden, S.A., "Identifying Multiscale Statistical Models Using the Wavelet Transform," SM Thesis, MIT, May 1991.
- Goodwin, G.C., R.J. Evass, R.L. Leal, and R.A. Feik, "Sinusoidal Disturbance Rejection with Application to Helicopter Flight Data Estimation," *IEEE Trans. Acoust., Speech, Signal Processing*, Vol. 34, June 1986, pp. 479-484.
- Isermann, R., "Process Fault Detection Based on Modeling and Estimation Methods—A Survey," *Automatica*, Vol. 20, 1984, pp. 387-404.
- Kim, M. and A.H. Tewfik, "Fast Multiscale Detection in the Presence of Fractional Brownian Motions," *Proc. SPIE Conf. on Advanced Algorithms and Architecture for Signal Processing V*, San Diego, CA, July 1990.
- Korn, J. and N.R. Sandell, "Tool Wear Sensing and Failure Detection via Modern Estimation Theory," ALPHATECH Technical Report TR-131, Burlington, MA, March 1982.
- Korn, J. and S.W. Gully, "On-Line Wear Estimation and Failure Detection of Oil-Well Drill Bits," ALPHATECH Technical Report TR-271, Burlington, MA, November 1985.
- Lawton, W.M., "Wavelet Discretization Methods for Surface Estimation and Reconstruction," *SPIE/SPSE Symp. on Elec. Imaging Sci. and Tech.*, Santa Clara, CA, February 1990.
- Le Vey, G., "Analyse Modale et Surveillance Vibratoire des Machines Tournantes," PhD Thesis, University of Rennes, France, 1988.
- Ljung, L. and T. Söderström, *Theory and Practice of Recursive Identification*, MIT Press, Cambridge, MA, 1983.
- Mallat, S. and W.L. Hwang, "Singularity Detection and Processing with Wavelets," *IEEE Trans. Inform. Theory*, Vol. 38, No. 2, March 1992, pp. 617-643.
- Mallat, S.M. and S. Zhang, "Compact Image Coding from Edges with Wavelets," *ICASSP-91*.
- Mallat, S.M., "Zero-Crossings of a Wavelet Transform," *IEEE Trans. Inform. Theory*, July 1981.
- Moustakides, G., M. Basseville, A. Benveniste, and G. Le Vey, "Diagnosing Mechanical Changes in Vibrating Systems," IRISA (Institut de Recherche en Informatique et Systèmes Aléatoires) Report 436, Rennes, France, October 1988.
- Pati, Y.C. and P.S. Krishnaprasad, "Analysis and Synthesis of Feedforward Neural Networks Using Discrete Affine Wavelet Transforms," preprint, Univ. Maryland, 1991.
- Pentland, A., "Finite Element and Regularization Solutions Using Wavelet Bases," MIT Media Lab Vision and Modeling Group TR-143, June 1990.
- Porat, B. and B. Friedlander, "Adaptive Detection of Transient Signals," *IEEE Trans. Acoust., Speech, Signal Processing*, Vol. 34, December 1986.
- Rougée, A., "Détection de Changements dans les Paramètres AR d'un Processus ARMA Vectoriel: Application à la Surveillance des Vibrations," PhD Thesis, University of Rennes, 1985.

ALPHATECH, INC.

- Tewfik, A.H. and M. Kim, "Correlation Structure of the Discrete Wavelet Coefficients of Fractional Brownian Motions," *IEEE Trans. Inform. Theory*, Vol. 38, No. 2, March 1992, pp. 904-909.
- Tuteur, F.B., "Wavelet Transformations in Signal Detection," *ICASSP-88*.
- Weiss, J.L., and J.Y. Hsu, "Design and Evaluation of a Failure Detection and Isolation Algorithm for Restructurable Control Systems," NASA CR-178213, NASA Langley Research Center, March 1987.
- Weiss, J.L., and J.Y. Hsu, "Expanded Envelope Concepts for Aircraft Control-Element Failure Detection and Identification," NASA CR-181644, NASA Langley Research Center, June 1988.
- Weiss, J.L., J.L. Stifel, and K.S. Govindaraj, "Flight Test Results of a Control Element Failure Detection and Isolation Algorithm," *Proc. National Aerospace and Electronics Conf.*, Dayton, OH, May 1986.
- Wickerhauser, M.V., "Acoustic Signal Compression with Wave Packets," preprint.
- Wornell, G.W. and A.V. Oppenheim, "Estimation of Fractal Signals from Noisy Measurements Using Wavelets," *IEEE Trans. Signal Processing*, to appear.
- Wornell, G.W. and A.V. Oppenheim, "Wavelet-Based Representations for a Class of Self-Similar Signals with Application to Fractal Modulation," *IEEE Trans. Inform. Theory*, Vol. 38, No. 2, March 1992, pp. 785-800.
- Wornell, G.W., "A Karhunen-Loève-Like Expansion for $1/f$ Processes via Wavelets," *IEEE Trans. Inform. Theory*, Vol. 36, No. 9, July 1990, pp. 859-861.
- Zhang, Q. and A. Benveniste, "Approximation by Nonlinear Wavelet Networks," *ICASSP-91*, Toronto, May 1991.

APPENDIX A

THE CONTINUOUS WAVELET TRANSFORM

This appendix presents the basics of the Continuous Wavelet Transform, which underlies our methodology for selecting features.

A.1 WAVELET BASES

Wavelets are a new approach to an old problem—building complicated functions out of simple elements. Fourier analysis builds complicated functions out of sine and cosine functions. Wavelets use functions with limited time extent, so that they can better represent time-localized aspects of a function than can a sum of infinite-duration sines and cosines.

All wavelet analyses are based on dilations, contractions, and translations of a basic *mother wavelet*. If the dilations, contractions, and translations are orthogonal to one another, then the wavelets form an orthonormal basis which is complete in many cases. One unique characteristic of wavelet analysis is that there are an infinite number of choices for a mother wavelet, allowing one to continuously vary the tradeoff between time and frequency localization. Figure A-1 shows the Haar wavelet, on the left, and the Kiang wavelet, on the right. Figure A-2 shows dilated and contracted translates of the Haar wavelet.

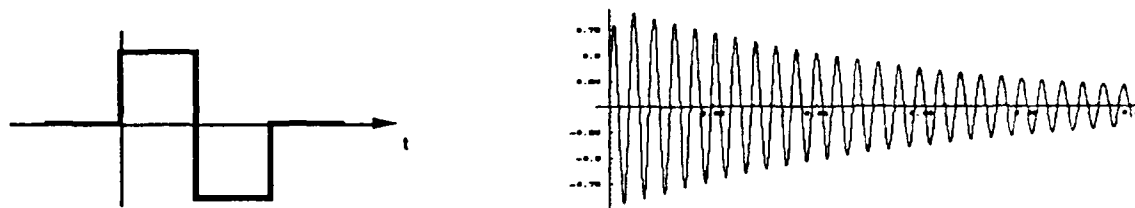


Figure A-1. The Haar and Kiang Wavelets

In its most general form, a mother wavelet is any essentially time- and band-limited function of t , subject to the uncertainty principle limitations. (The uncertainty principle states that good time localization is obtained at the expense of frequency localization, and vice versa.)

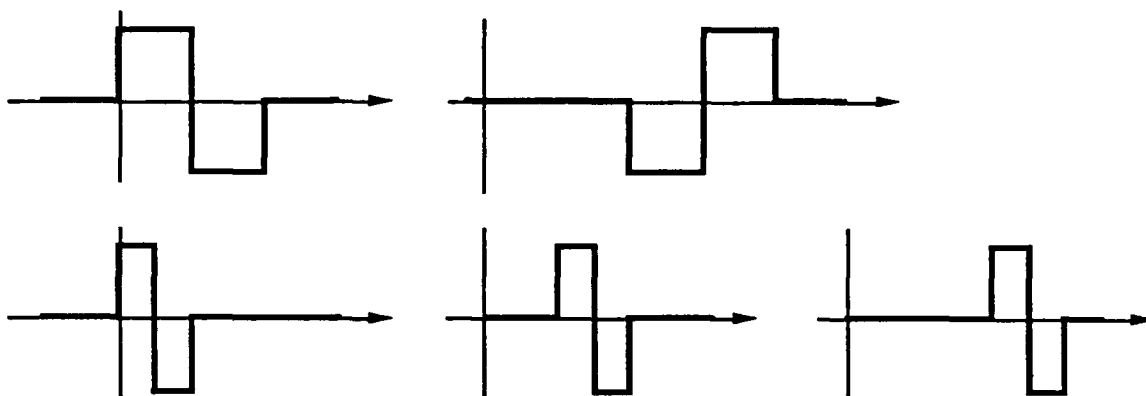


Figure A-2. Dilated Translates of the Haar Wavelet

An affine wavelet family is obtained from dilations and translations of the mother wavelet. Affine wavelets can be either continuous or discrete (usually dyadic). Dyadic wavelet families dilate by powers of two, and translate by integral multiples of power of two. Continuous wavelet families dilate by arbitrary scale factors, and translate by arbitrary amounts.

A.2 WAVELETS AND SPECTRA

Each mother wavelet has a characteristic footprint in time/frequency space—a region where it is sensitive to energy. Dilate it (or contract it) by a factor of two, and this region expands (or contracts) by a factor of two along the time axis, and translates by an octave down (or up) along the frequency axis. Translate it, and the footprint moves an equal amount along the time axis. Take a set of dilations, contractions, and translations that cover all of time/frequency space, and you have a complete basis set. Figure A-3 illustrates a typical subdivision by wavelets of the time-frequency plane.

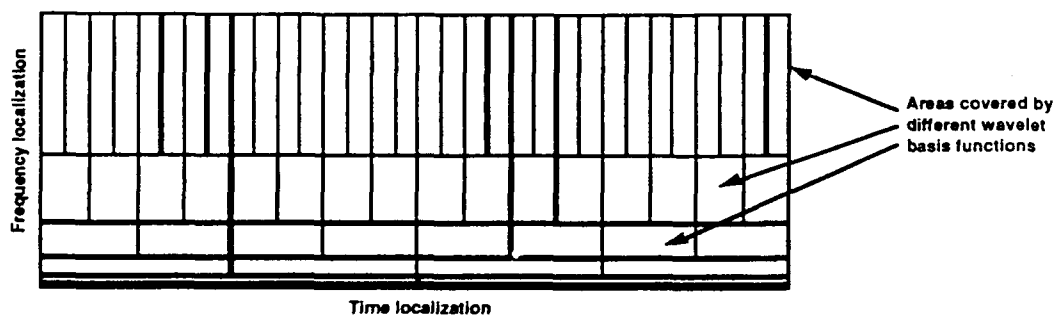


Figure A-3. Typical Subdivision by Wavelets of the Time-Frequency Plane

The exciting discoveries that kindled the recent interest in wavelets concern the existence of such complete bases that are also orthonormal, and for which the mother wavelet has finite support (is non-zero over a finite length of time).

A.3 WAVELET TRANSFORMS

Because there are an infinite number of mother wavelets, there are an infinite number of wavelet transforms. By varying the choice of the mother wavelet, one can get wavelet transforms that differ in both time and frequency localization.

An affine wavelet transform is the set of coefficients that multiply elements of a wavelet family in order to represent a time function. Affine wavelet transforms can be either continuous or discrete. Continuous wavelet transforms yield a complex-valued function of time and space (frequency). Discrete (usually dyadic) wavelet transforms yield a finite number of coefficients for an essentially bounded region of time and scale (frequency). All wavelet transforms contain implicit or explicit feature detectors (one for each basis function). Figure A-4 presents a classification of affine and non-affine wavelets based on their support (columns) and extent of their filter realizations (rows).

| Weyl-Heyerdahl wavelets (non-affine) | | | } Historical interest |
|--------------------------------------|---------------------------|----------------------------|-----------------------|
| | Bounded | Semi-infinite | |
| Finite | DFT Hanning Hamming | Laplace (limited) | |
| Infinite | | Bessel | Gabor Weyl |
| Affine wavelets | | | } Recent results |
| | Bounded | Semi-infinite | |
| Finite | Haar Daubechies | Laplace (limited) Klang | |
| Infinite | | Bessel | "Mexican Hat" |

Figure A-4. Classification of Wavelets

Wavelet selection affects preprocessor design. Efficient real-time feature extraction imposes constraints on possible mother wavelets. We require causality and a finite dimensional

realization of the wavelet generator. In this effort, we constrained the choice of mother wavelet based on our need to implement a feature extractor without new leaps forward in electronics technology. In particular, we limited our choices to those for which corresponding filters have a finite dimensional realization. All of the wavelets with finite support possess this property, but must be very long in order to localize the narrowband energy so obvious in the gearbox data. Therefore, we selected a wavelet with semi-infinite support, so that it has a causal realization, and a low-dimensional implementation. This wavelet was derived from auditory nerve response data collected by Kiang in the 1960s, and we have honored him by appropriating his name for the wavelet.

A.4 SIMPLE EXAMPLES OF CONTINUOUS WAVELET TRANSFORMS

This section presents color images of Continuous Wavelet Transforms (CWTs) of some basic functions to give the reader greater insight into the time-frequency representation of signals provided by the CWT based on the Kiang wavelet. In these images, the frequency scale is logarithmic and runs vertically, increasing to the top, with frequency divisions corresponding to octaves from 16 Hz to 16 kHz. The time scale runs horizontally, increasing to the right, with time divisions 62.5 msec wide. Hue encodes the log magnitude of the CWT (blue = low, red = high). Phase information is ignored.

A.4.1 Pulse and Sine Wave

The left image in Plate M is a wavelet transform, using the Kiang wavelet, of a 1 msec pulse sampled at 48 kHz. Note the nulls at multiples of 1 kHz, reflecting the fact that the Kiang wavelet is highly oscillatory and thus almost orthogonal to pulses that extend over an integral number of complete cycles. Note that the finer scales allow very precise placement of the time that the pulse occurs, and the absence of windowing effects.

The right image is a wavelet transform of a stepped sine wave. Note that initial transients quickly give way to a very tight localization of the center frequency of the sine. Note also that the transients decay more slowly for the coarser scales at the right of the figure.

A.4.2 Superposition Examples

The left image in Plate N is a wavelet transform of the sum of the two functions in Plate M. It provides clear evidence that a single transform can localize transient events well in time, while at the same time localizing stationary frequencies.

The right image is a wavelet transform of two stepped sine waves of identical amplitude and similar frequency. It provides a dramatic visualization of beat effects, as the pattern of the peak is a periodic variation between two separate, lower-energy signals and a single, higher-energy signal. As the difference between center frequencies increases, proportionally more of each beat cycle is occupied by the area with two distinct frequency peaks. Note that the detail of the beat structure is not typically present in sonograms, lofargrams, or waterfall displays—and it is this visibility into time/frequency variations of signal structure that is the advantage of the CWT.

A.4.3 Noise Examples

The left image in Plate O is a wavelet transform of a white Poisson process emitting 1-msec pulses, with a mean interarrival time of 10 msec. Note the clear separation between pulses apparent at the finer scales at the left of the image, in contrast to the random texture at lower scales at the right. There is clearly no structure to this signal that is localized in frequency.

The right image is a wavelet transform of a white Gaussian process. The apparent concentration of energy at the finer scales (higher frequencies) is due to the fact that the bandwidths of wavelets inevitably increase as they are contracted. Thus a process with equal energy at each frequency in a Fourier transform has exponentially increasing power as frequency increases in a wavelet transform.

APPENDIX B

BASIC MATHEMATICAL ASPECTS OF THE CWT

This appendix presents a summary of some basic mathematical aspects of the Continuous Wavelet Transform (CWT). For a more detailed treatment the reader is referred to Grossman et al. (1989), Kronland-Martinet et al. (1987).

B.1 ANALYZING WAVELETS

Suppose that the function $g(t)$, generally complex-valued, satisfies the following conditions:

- i) $g(t)$ is square-integrable, that is, it has finite energy

$$\int |g(t)|^2 dt < \infty$$

- ii) $\int |\hat{g}(\omega)|^2 d\omega / |\omega| < \infty$

where $\hat{g}(\omega)$, its Fourier transform, is defined as

$$\hat{g}(\omega) \equiv \frac{1}{\sqrt{2\pi}} \int e^{-i\omega t} g(t) dt.$$

Then $g(t)$ is called an *analyzing wavelet*.

In practice, however, additional conditions are imposed, such as:

- iii) its Fourier transform is differentiable; in such case, condition ii) implies that

$$\hat{g}(0) = 0, \text{ i.e., } \int g(t) dt = 0, \text{ and thus } g(t) \text{ oscillates around zero,}$$

iv) $g(t)$ is well localized in time, and $\hat{g}(\omega)$ is well localized in frequency, both subject to the limitations imposed by the uncertainty principle.

The family of continuous wavelets associated with the analyzing or *mother wavelet* $g(t)$ is defined by its dilates and translates, that is, by functions of the form

$$g^{(b,a)}(t) \equiv \frac{1}{\sqrt{a}} g\left(\frac{t-b}{a}\right)$$

where b , the *translation parameter*, is a real number, and a , the *scale parameter*, is a positive real number. The factor $1/\sqrt{a}$ ensures that the norms of $g(t)$ and $g^{(b,a)}(t)$ are equal (usually equal to unity). The norm of $g(t)$ is defined as

$$\|g\|^2 \equiv \int |g(t)|^2 dt$$

B.2 THE CONTINUOUS WAVELET TRANSFORM OF A SIGNAL

The CWT of a real-valued, continuous, deterministic signal $s(t)$ with respect to the analyzing wavelet $g(t)$ is the function $S(b,a) = S_g(b,a)$ defined on the open half-plane (b,a) as

$$S(b,a) \equiv \frac{1}{\sqrt{a}} \int \bar{g}\left(\frac{t-b}{a}\right) s(t) dt = \sqrt{a} \int \hat{g}(a\omega) \hat{s}(\omega) e^{ib\omega} d\omega$$

where $\bar{g}(t)$ is the complex conjugate of $g(t)$.

Two important properties of the correspondence between $s(t)$ and $S(b,a)$ are:

1) *Independence of choice of time origin*

If $s(t)$ is shifted in time by t_0 , (say, $s(t) \rightarrow s(t-t_0)$), then $S(b,a)$ is transformed into $S(b-t_0, a)$.

2) *Conservation of energy*

If $s(t)$ is a signal of finite energy, then

$$\int s(t)^2 dt = \frac{1}{c_s} \iint |S(b,a)|^2 \frac{da db}{a^2}$$

where

$$c_s \equiv 2\pi \int_{-\infty}^{\infty} \frac{|\hat{g}(\omega)|^2}{\omega} d\omega.$$

Since the CWT of a signal is generally complex-valued, it can be expressed as

$$S(b,a) = |S(b,a)| e^{i\varphi(b,a)}$$

where $|S(b,a)|$ is the modulus and $\varphi(b,a)$ is the phase. Both provide information about the signal $s(t)$. For instance, abrupt changes in the signal or its derivatives can under suitable circumstances

be seen on its transform. A discontinuity appears as a localized increase in the modulus $|S(b,a)|$ for small a , around a point b_0 since a discontinuity contains high frequencies. A discontinuity is also indicated by the convergence of lines of constant phase towards a point at the edge of the (b,a) half-plane.

There are many features of the signal that can be seen on $|S(b,a)|$ and which are independent of the choice of analyzing wavelet. These features often involve the phase $\varphi(b,a)$ (Grossman et al, 1989). In the Phase I effort, information only from the modulus was used. For Phase II we plan to examine phase information for the different faults to see whether it provides additional significant features for improving the classifier's performance.

Since the CWT is essentially a convolution between the signal and each wavelet, it can be computed rather straightforwardly by filtering the signal data samples with an appropriate digital filter. The digital filter corresponding to the Kiang wavelet used in the Phase I effort has a causal, finite dimensional realization.

A more intuitive treatment of the CWT and examples of the CWT of simple signals are presented in Appendix A.